

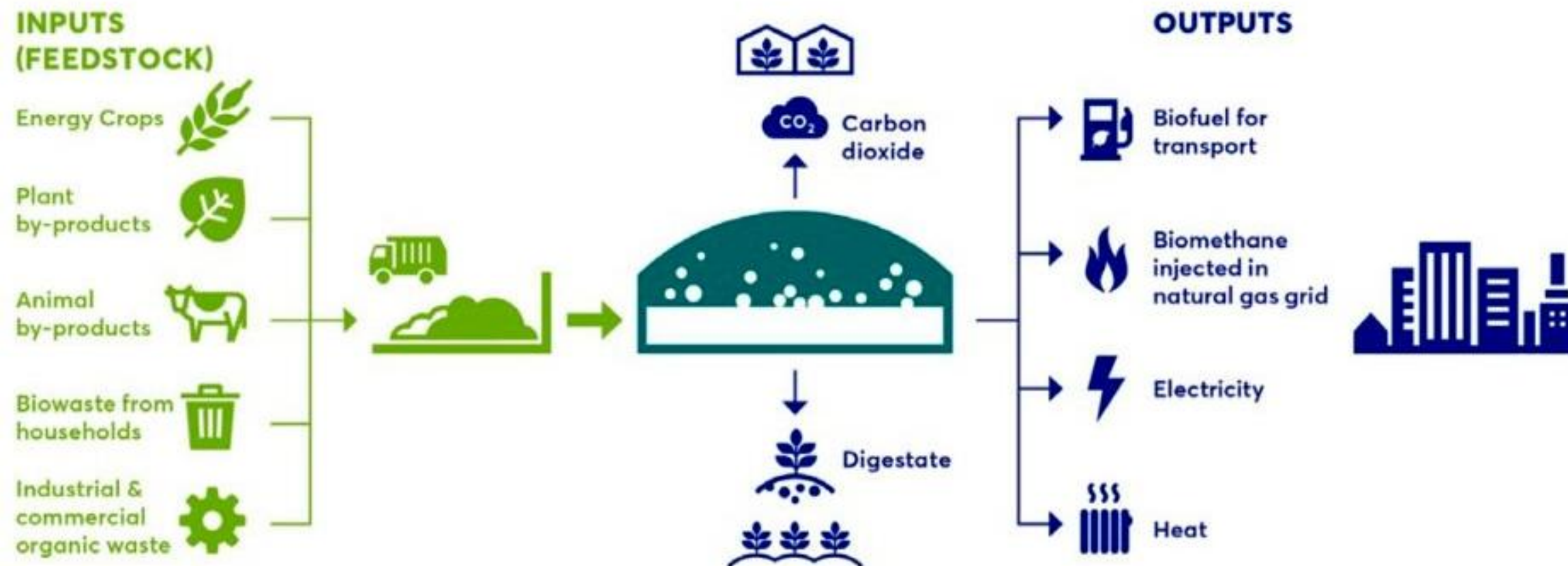
Catalytic Reaction and Reactor Engineering for Bio-Gas Valorization

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biogas

biogas = CH₄ (biomethane, ~50-70%) + CO₂ (~24-45%)



what if we could transform it into chemicals?

biogas to chemicals

- reactions

- CH_4

- steam reforming

- pyrolysis

- oxidative coupling

- CO_2

- dry reforming (with CH_4)

- hydrogenation

- reverse Boudouard

- reactors

- exothermicity

- multitubular

- fluidized bed

- endothermicity

- fired furnaces

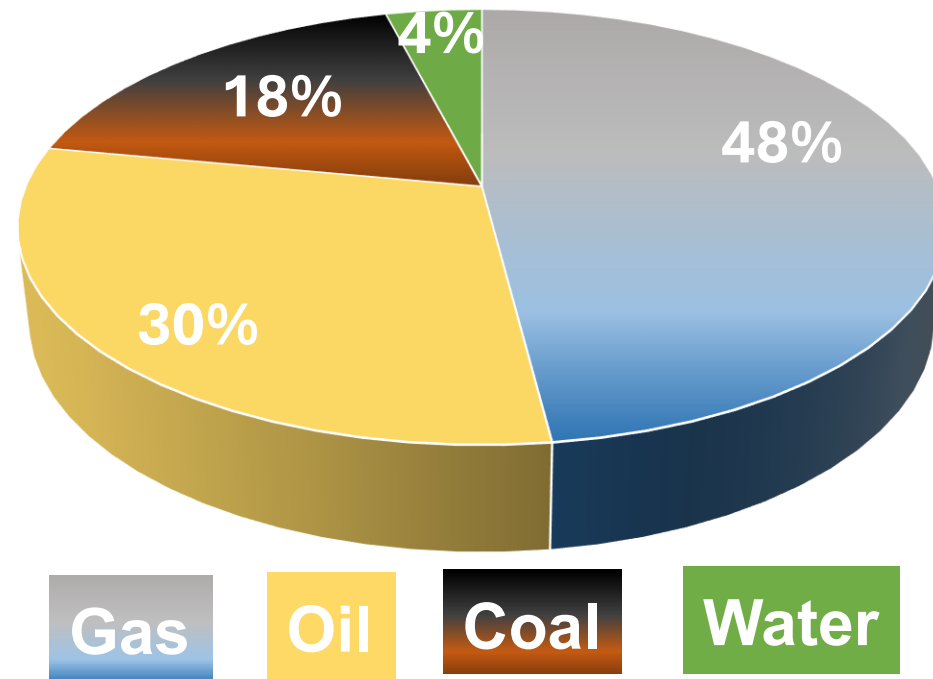
- electrification

outline

- introduction
- catalytic reaction engineering
 - hydrogen production/methane pyrolysis
 - gas phase vs surface reactions/catalyst descriptors
- catalytic reactor engineering
 - electrification/ElectroThermal Fluidized Bed reactor (ETFB)
 - ETFB reactor model
- conclusions & perspectives

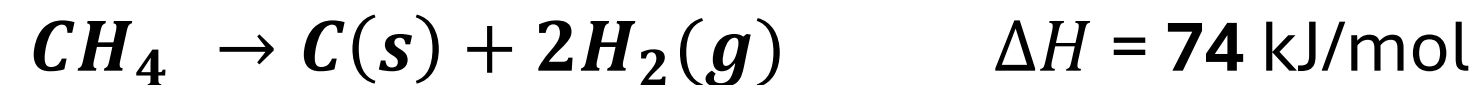
CH₄ conversion → H₂ production

H₂ production feedstocks



Technology	reaction	ΔH kJ/mol	cost (\$/kg)	GWP (kg CO ₂ eq)
Steam Methane Reforming SMR + CCS	$CH_4 + H_2O \leftrightarrow CO + 3H_2$	206	2.08	11.9
			2.27	3.7
Coal Gasification CG + CCS	$C + H_2O \leftrightarrow CO + H_2$	-130	1.34	22.9
			1.63	4.8
Electrolysis	$2H_2O \leftrightarrow 2H_2 + O_2$	285	>3	>0.7

Catalytic Methane Decomposition:

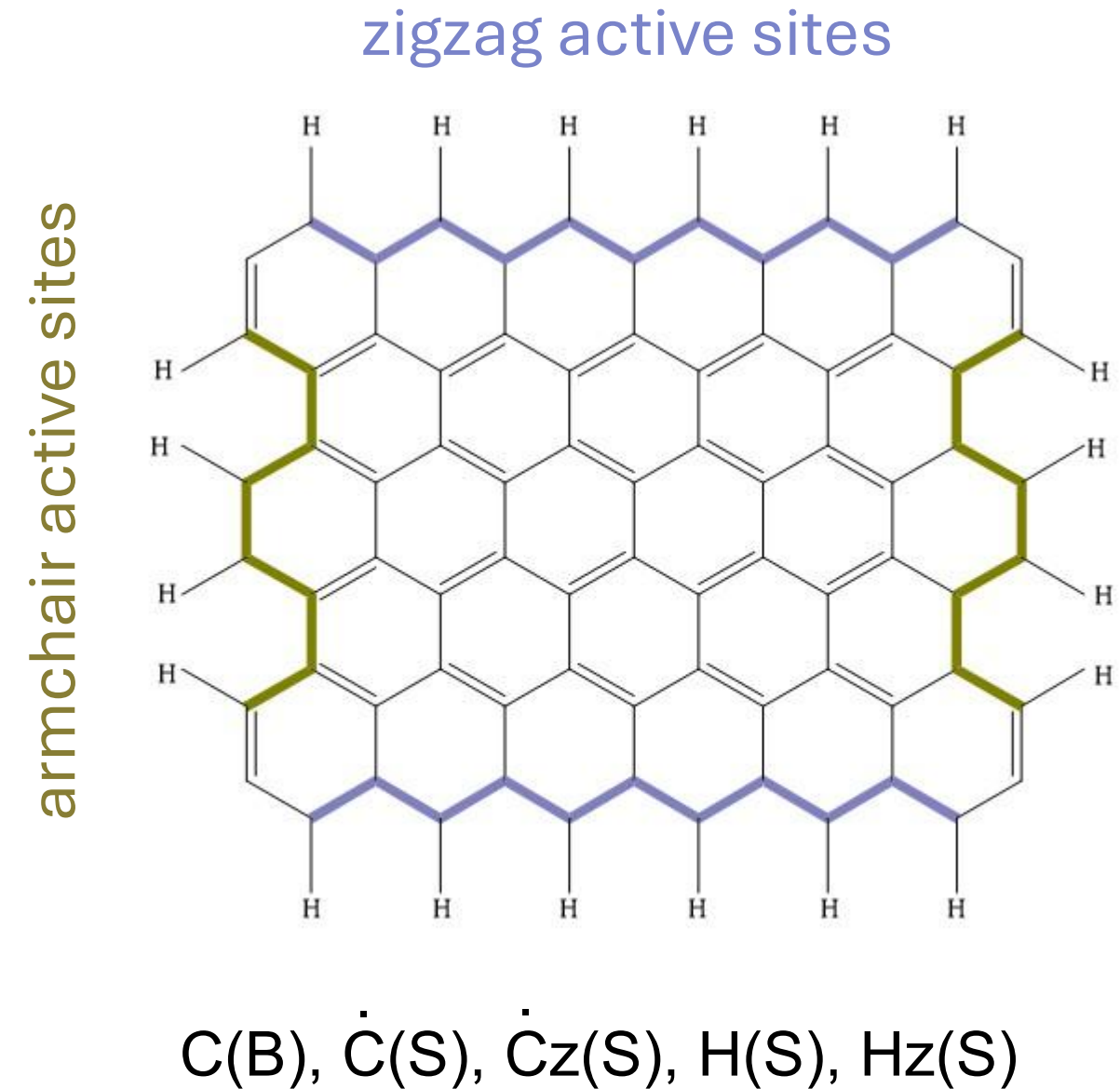


CDM on carbonaceous catalyst:

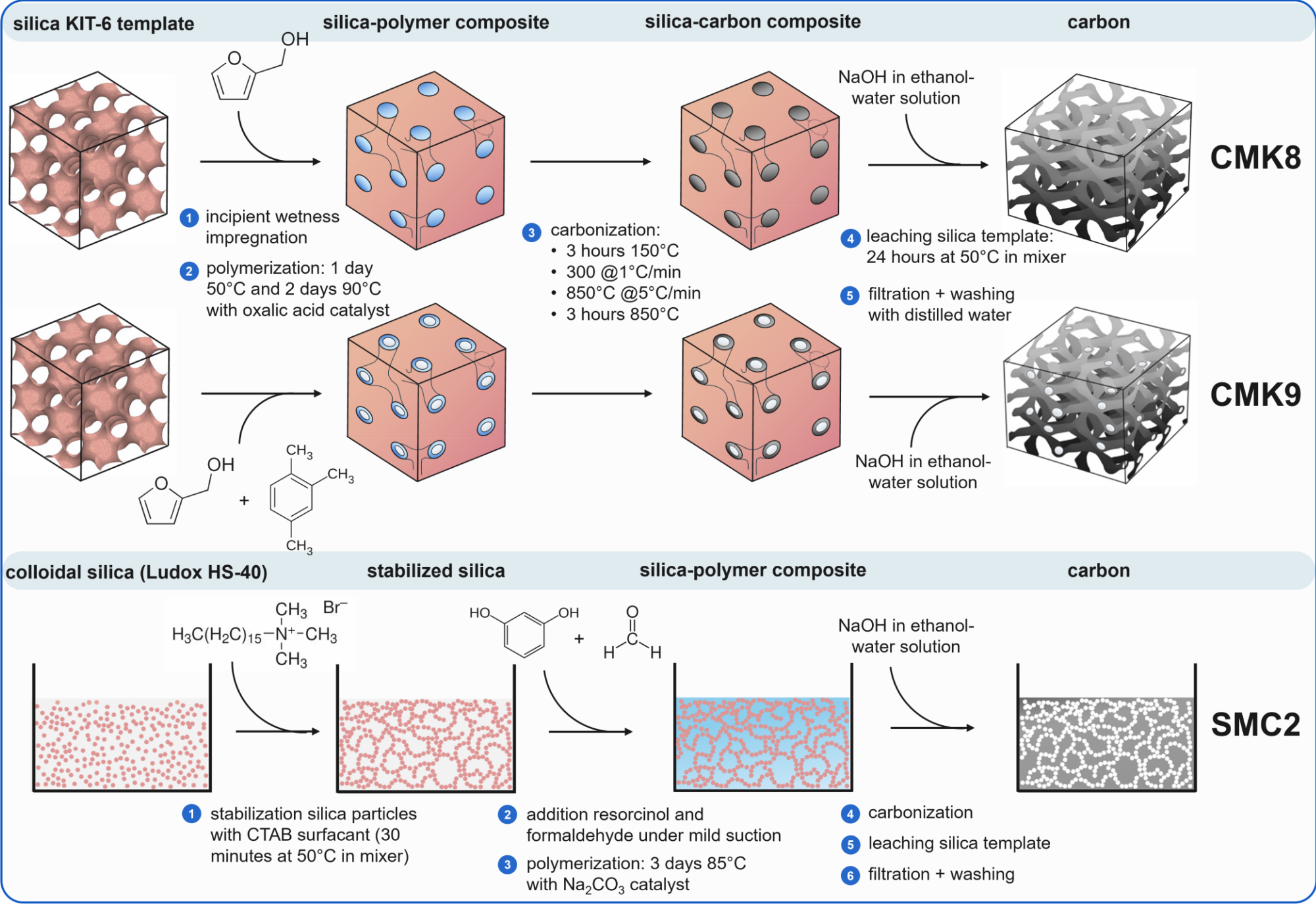
- ☐ less energy-intensive
- ☐ Less greenhouse gas emission
- ☐ Produces H₂ with high purity
- ☐ Cheap catalyst
- ☐ Sulfur-resistive catalyst

CH₄ pyrolysis

- gas phase reactions
 - AramcoMech 3.0
- surface reactions
 - Lacroix:
 - 66 species
 - 275 reactions
 - catalyst descriptors
 - ordered vs amorphous



carbonaceous materials synthesis

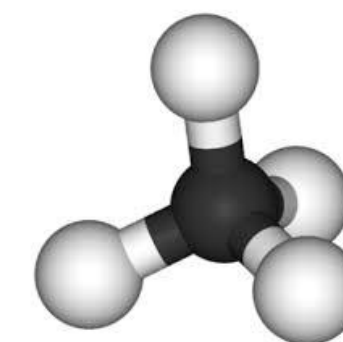
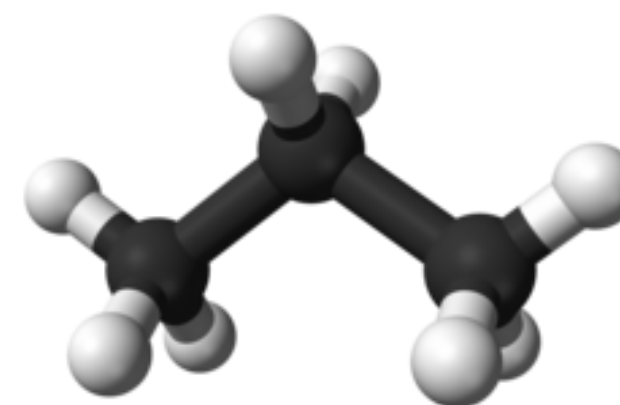
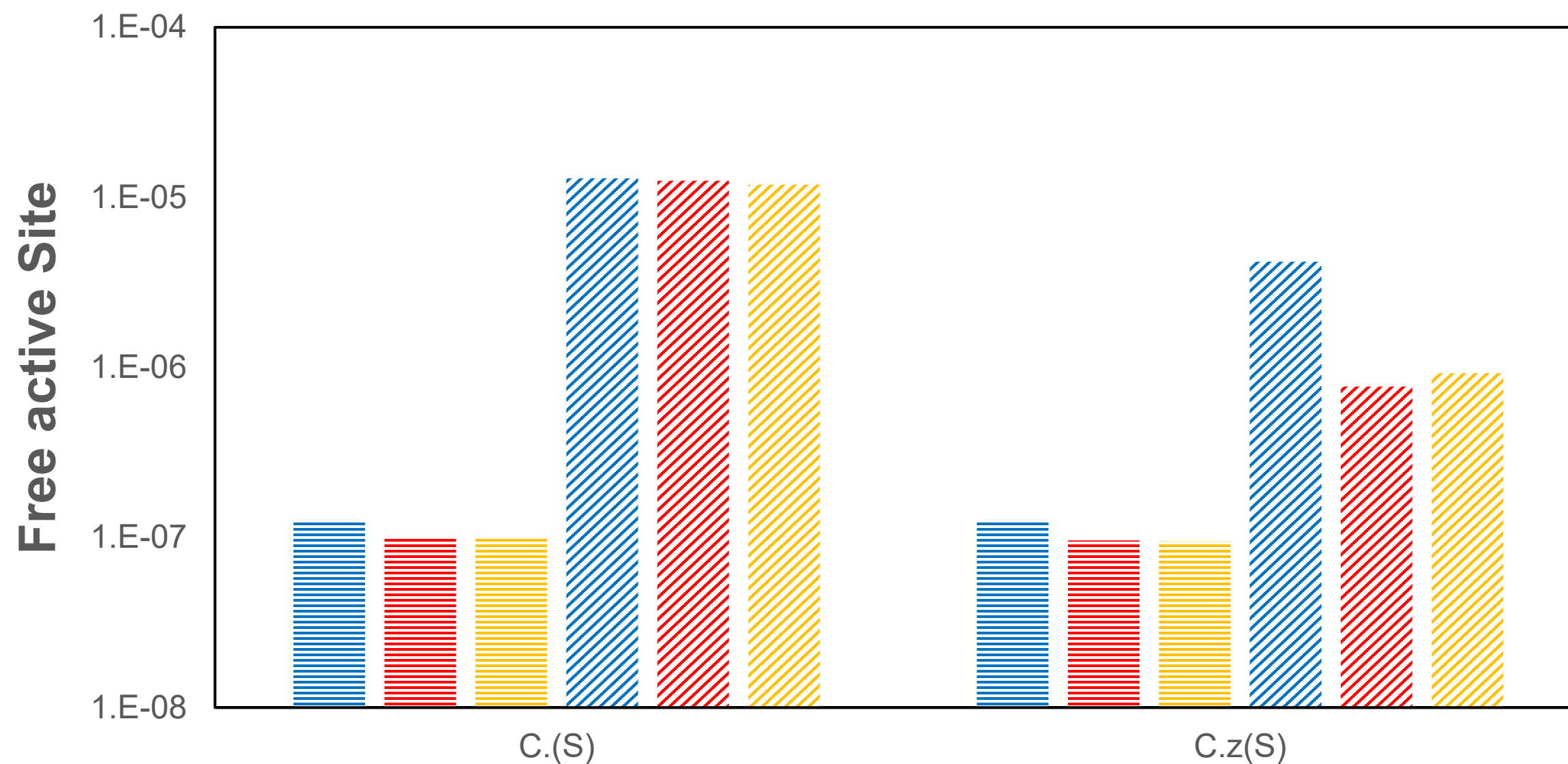


carbon black surface properties carbon black.			
	BP2000	V72	BP120
total number of active sites (g ⁻¹)	2 10 ¹⁹	1 10 ¹⁸	7 10 ¹⁷
active site density (mol/cm ²)	2.1 10 ⁻¹²	7.3 10 ⁻¹³	3.8 10 ⁻¹²
surface area (m ² /g)	1516	224	30.5

selected surface reactions

	surface reactions*	A_f	n_f (-)	Ea_f (kJ/mol)	A_r	n_r (-)	Ea_r (kJ/mol)
1.a	$C(B) + H(S) + \dot{H} \leftrightarrow \dot{C}(S) + H_2$	$5 \cdot 10^7$	1.8	70.2	$1.4 \cdot 10^7$	1.8	36.3
1.z	$C(B) + Hz(S) + \dot{H} \leftrightarrow \dot{C}z(S) + H_2$						
2.a	$C(B) + H(S) + C\dot{H}_3 \leftrightarrow \dot{C}(S) + CH_4$	$6.6 \cdot 10^{11}$	0	62.7	$1.4 \cdot 10^{12}$	0	30.5
2.z	$C(B) + Hz(S) + C\dot{H}_3 \leftrightarrow \dot{C}z(S) + CH_4$						
3	$C(B) + H(S) + C_2\dot{H}_5 \leftrightarrow \dot{C}(S) + C_2H_6$	$1 \cdot 10^{11}$	0	62.7	$5 \cdot 10^{11}$	0	10.8
4	$C(B) + H(S) + C_2\dot{H}_3 \leftrightarrow \dot{C}(S) + C_2H_4$	$1 \cdot 10^{11}$	0	54.3	$4.7 \cdot 10^{11}$	0	40.9
5.a	$C(B) + H(S) \leftrightarrow \dot{C}(S) + \dot{H}$	$1.7 \cdot 10^{16}$	0	470	$1 \cdot 10^{14}$	0	0
5.z	$C(B) + Hz(S) \leftrightarrow \dot{C}z(S) + \dot{H}$						
5.a**	$C(B) + H(S) \leftrightarrow \dot{C}(S) + \dot{H}$	$6.7 \cdot 10^{15}$	0	337.3	$1 \cdot 10^{14}$	0	0
5.z*	$C(B) + Hz(S) \leftrightarrow \dot{C}z(S) + \dot{H}$	$1 \cdot 10^{15}$	0	382	$1 \cdot 10^{14}$	0	0 ₈

relevance surface reactions (C_3H_8 vs CH_4)



BP2000-Lacroix

V72-Lacroix

BP120-Lacroix

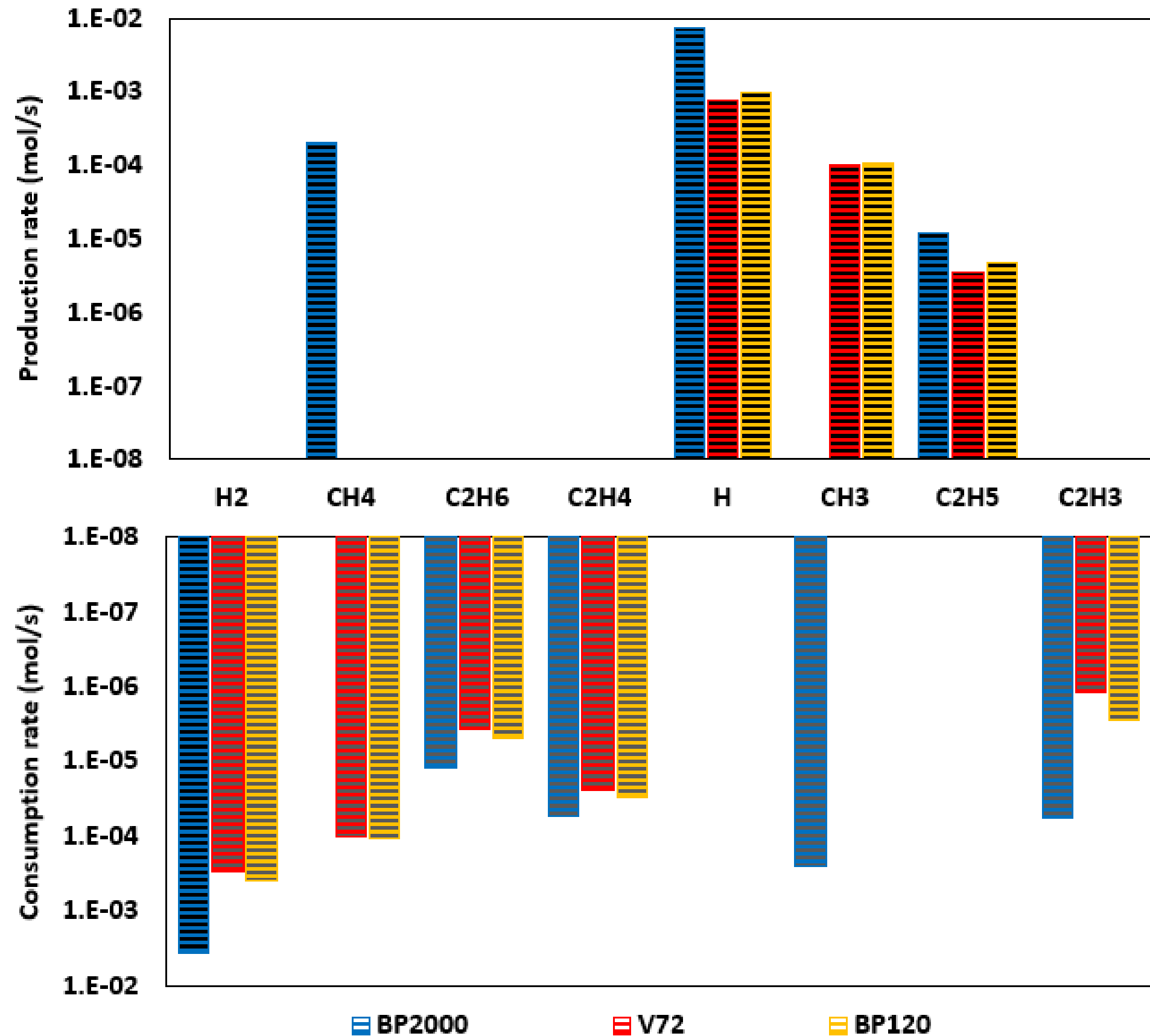
BP2000-This work

V72-This work

BP120-This work

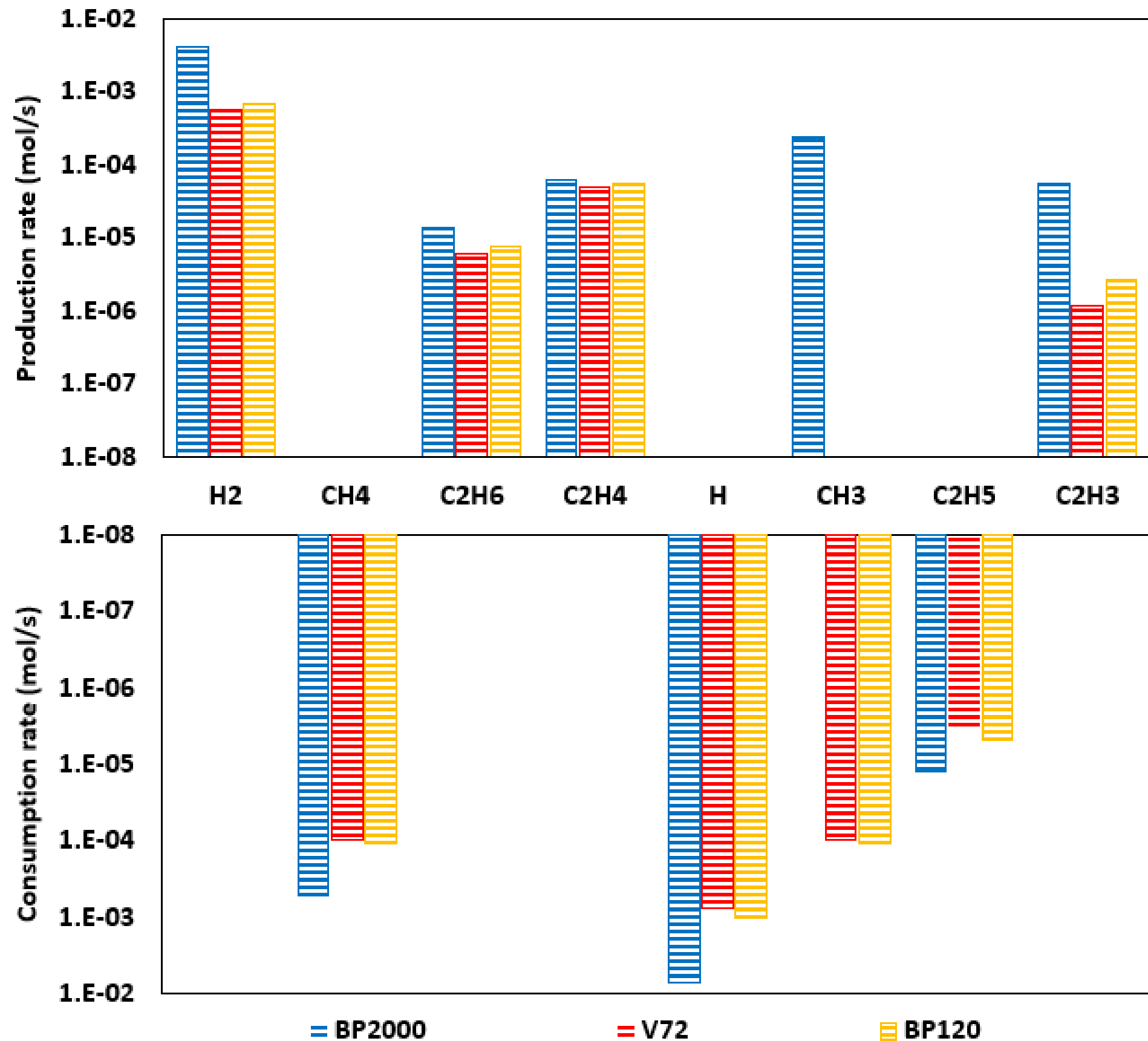
surface rates

- H radical production
- methyl radical:
 - consumption (large surface area)
 - production (low surface area)
- methane: reverse of methyl radical



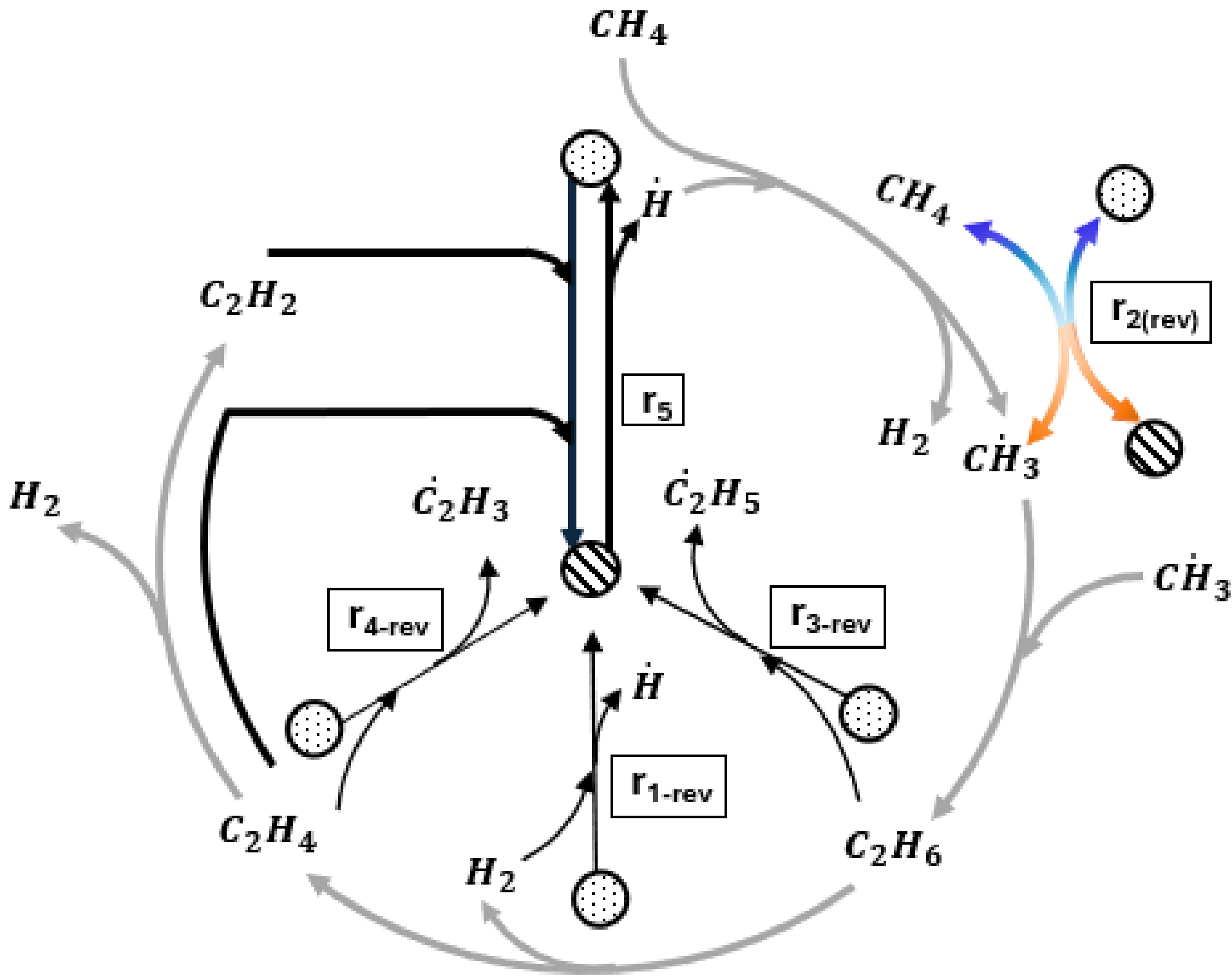
gas phase rates

- H radical reacts with CH_4 into H_2 and methyl radical
- methyl radical:
 - production (large surface area)
 - consumption (low surface area)
- methane: consumption only

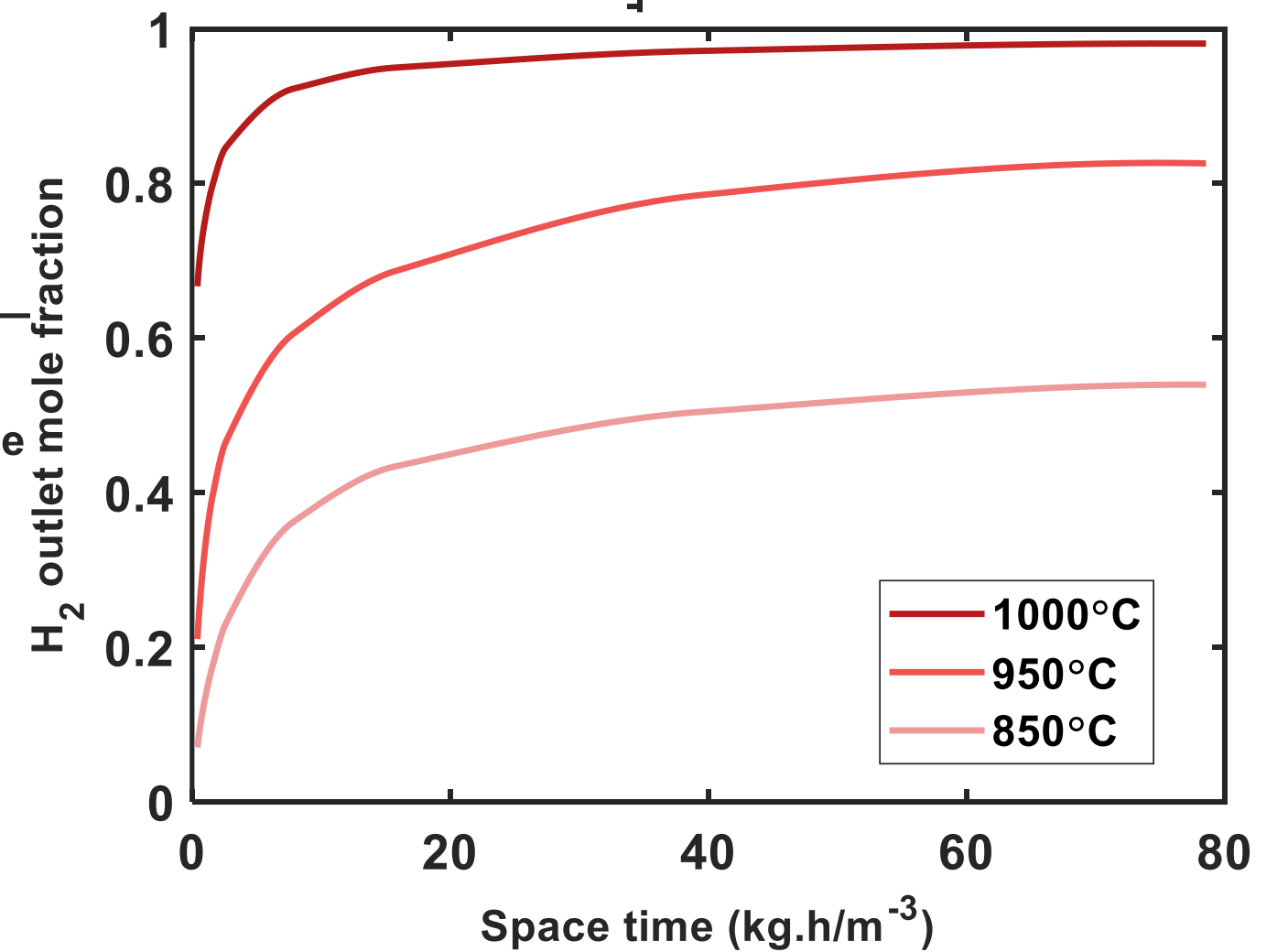
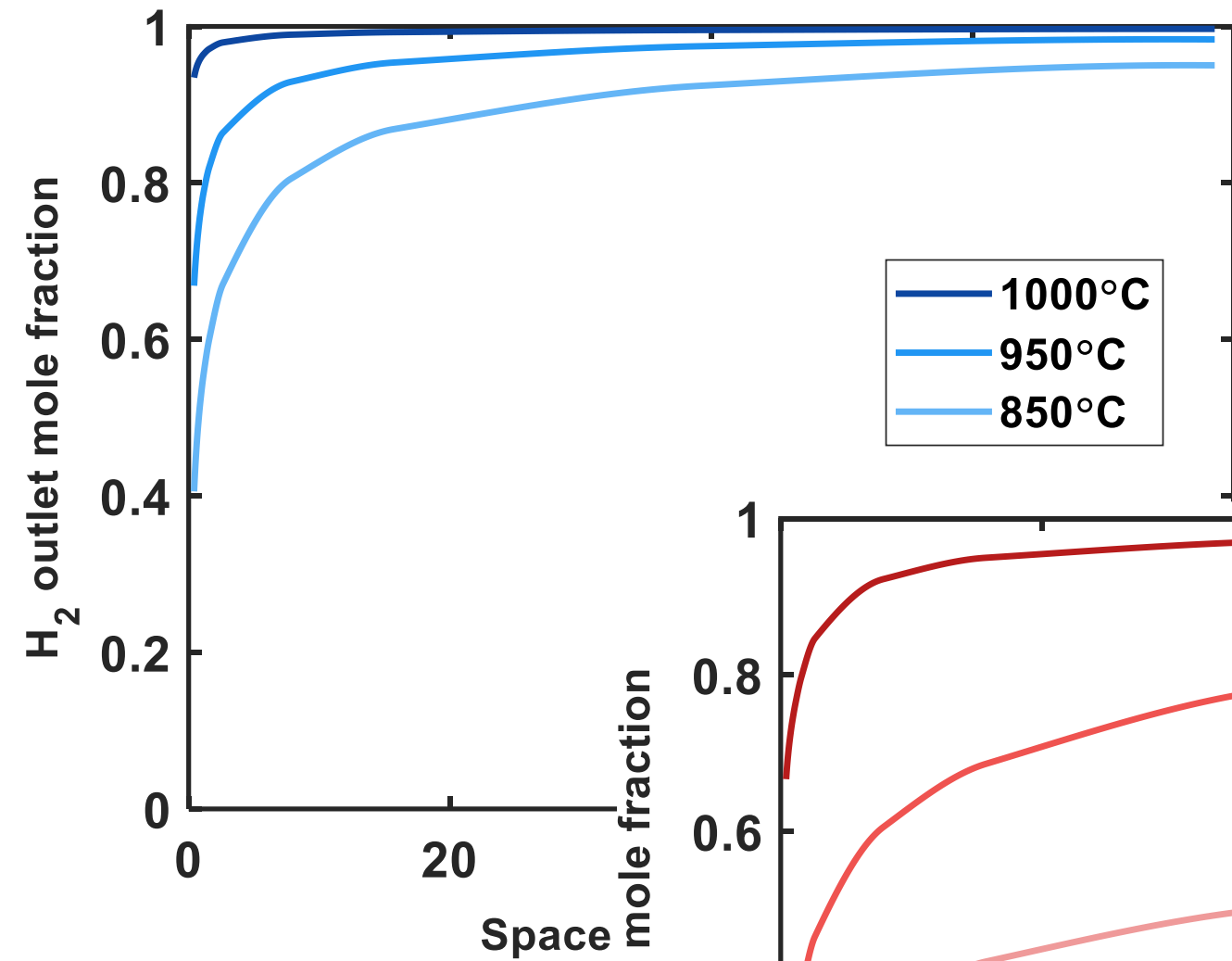
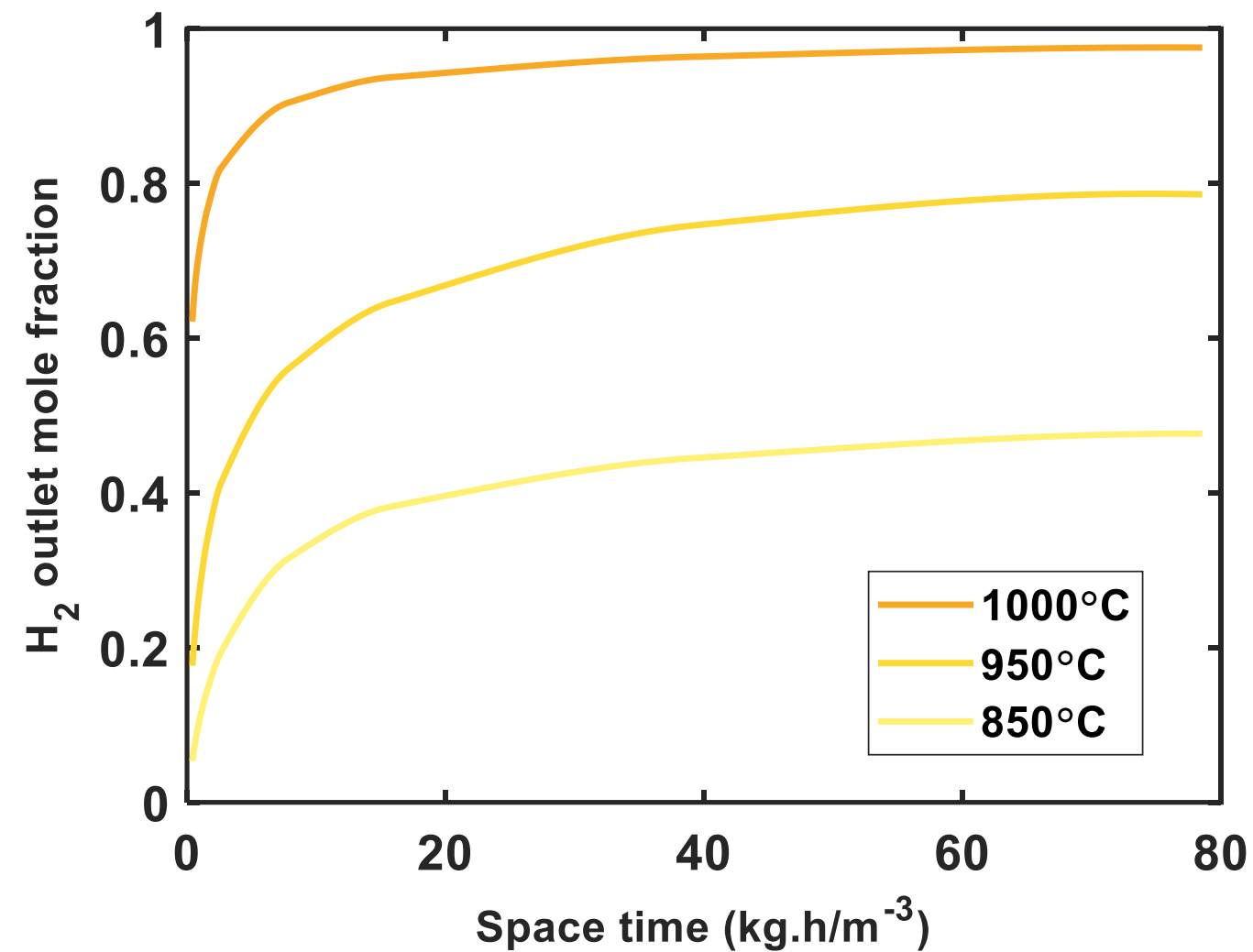


reaction pathway analysis

	surface reactions*
1.a	$C(B) + H(S) + \dot{H} \leftrightarrow \dot{C}(S) + H_2$
1.z	$C(B) + Hz(S) + \dot{H} \leftrightarrow \dot{C}z(S) + H_2$
2.a	$C(B) + H(S) + C\dot{H}_3 \leftrightarrow \dot{C}(S) + CH_4$
2.z	$C(B) + Hz(S) + C\dot{H}_3 \leftrightarrow \dot{C}z(S) + CH_4$
3	$C(B) + H(S) + C_2\dot{H}_5 \leftrightarrow \dot{C}(S) + C_2H_6$
4	$C(B) + H(S) + C_2\dot{H}_3 \leftrightarrow \dot{C}(S) + C_2H_4$
5.a	$C(B) + H(S) \leftrightarrow \dot{C}(S) + \dot{H}$
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5.a**	$C(B) + H(S) \leftrightarrow \dot{C}(S) + \dot{H}$
5.z*	$C(B) + Hz(S) \leftrightarrow \dot{C}z(S) + \dot{H}$



H₂ production over carbon catalysts

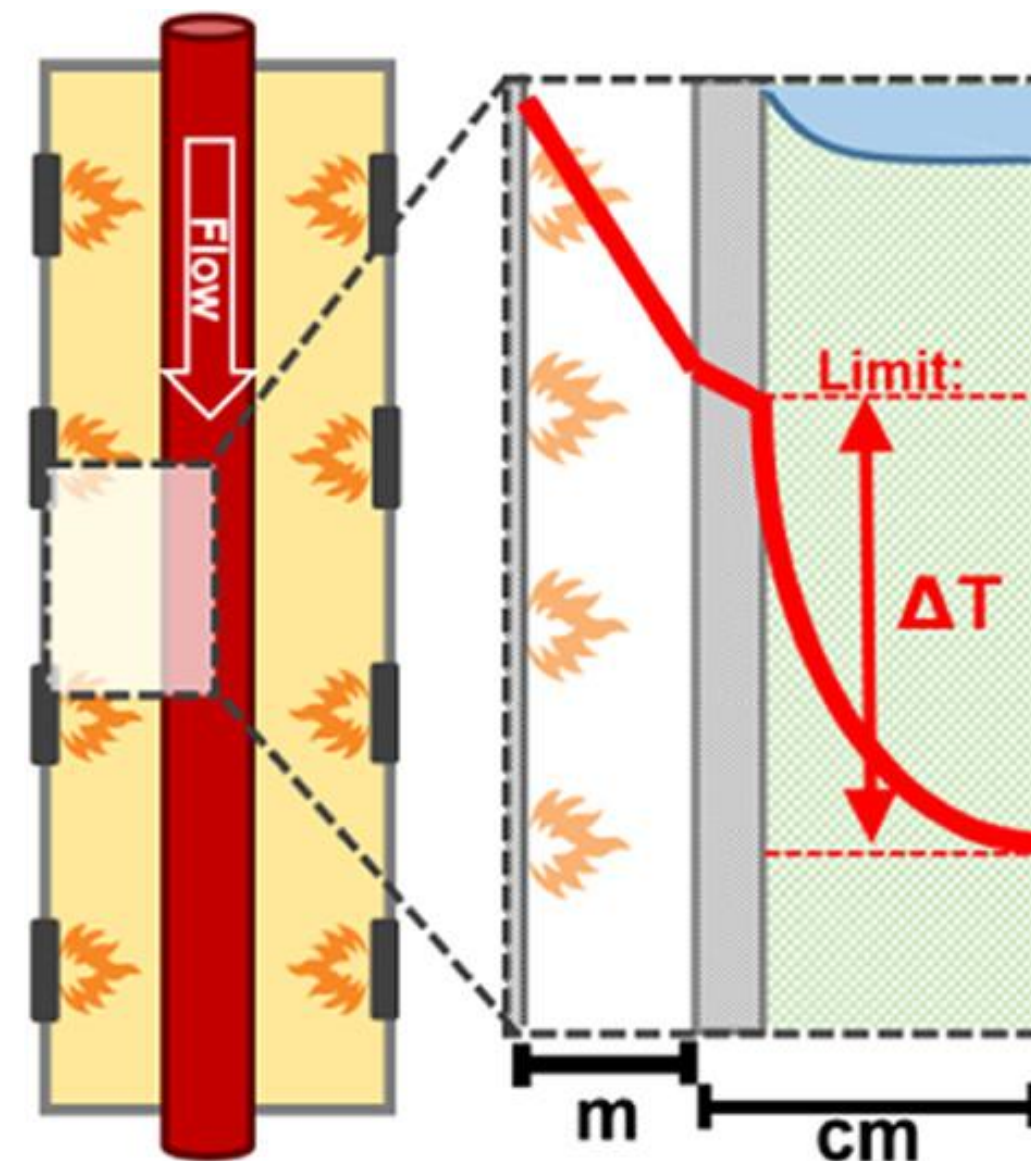
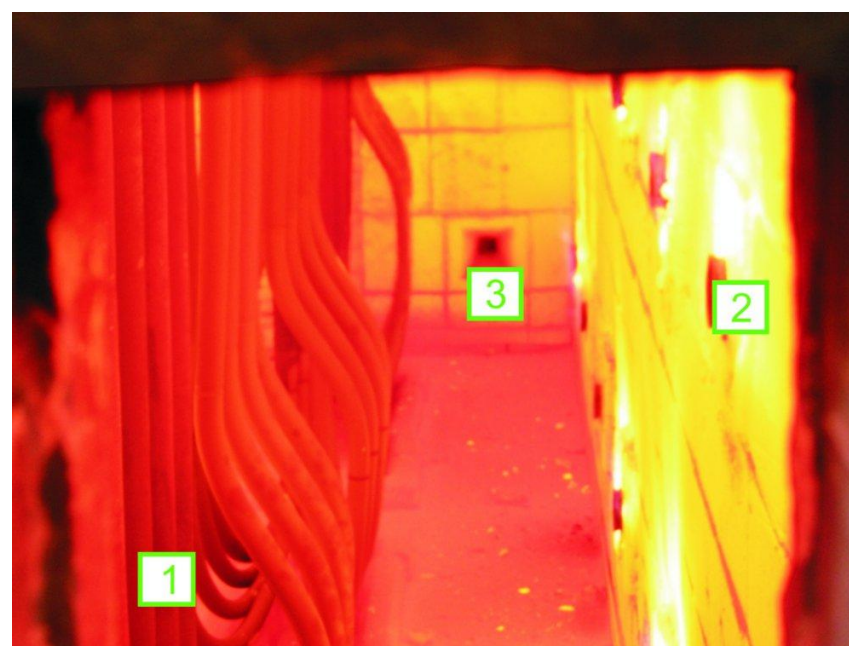


outline

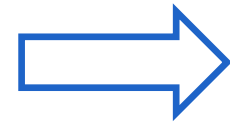
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(strongly) endothermic reactions

- heat transport focused reactor design
- narrow tubes
- fired furnace
- pronounced temperature gradients



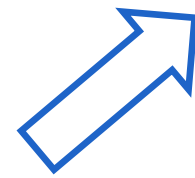
how can we enhance heat transfer?



heat containment

electrification

how can we do even better?



microwave



induction

**heating from
the inside**

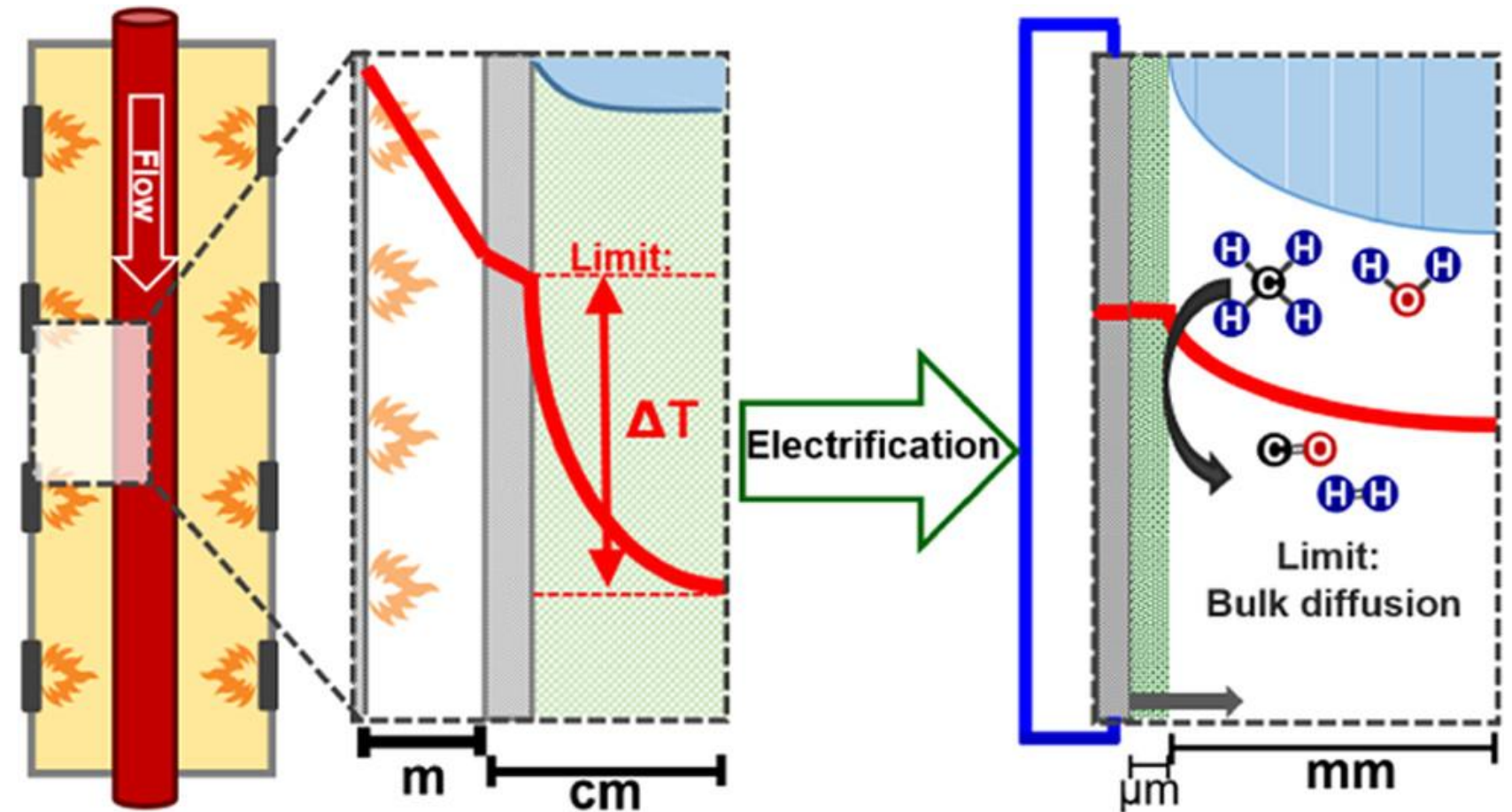


reactor electrification

electrical heating -> overcoming limitations of combustion in furnaces

advantageous in terms of:

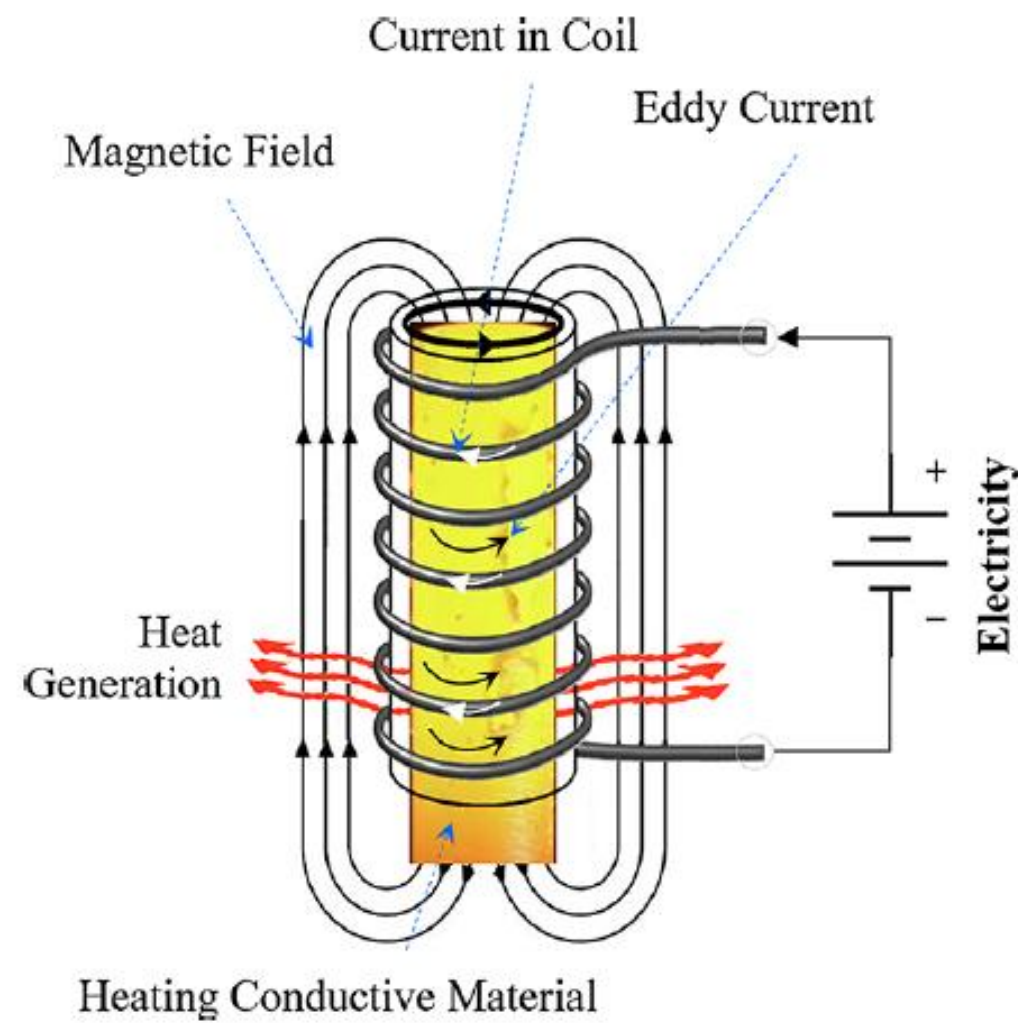
- energy efficiency
- process control
- safety and maintenance
- rapid heating
- ...



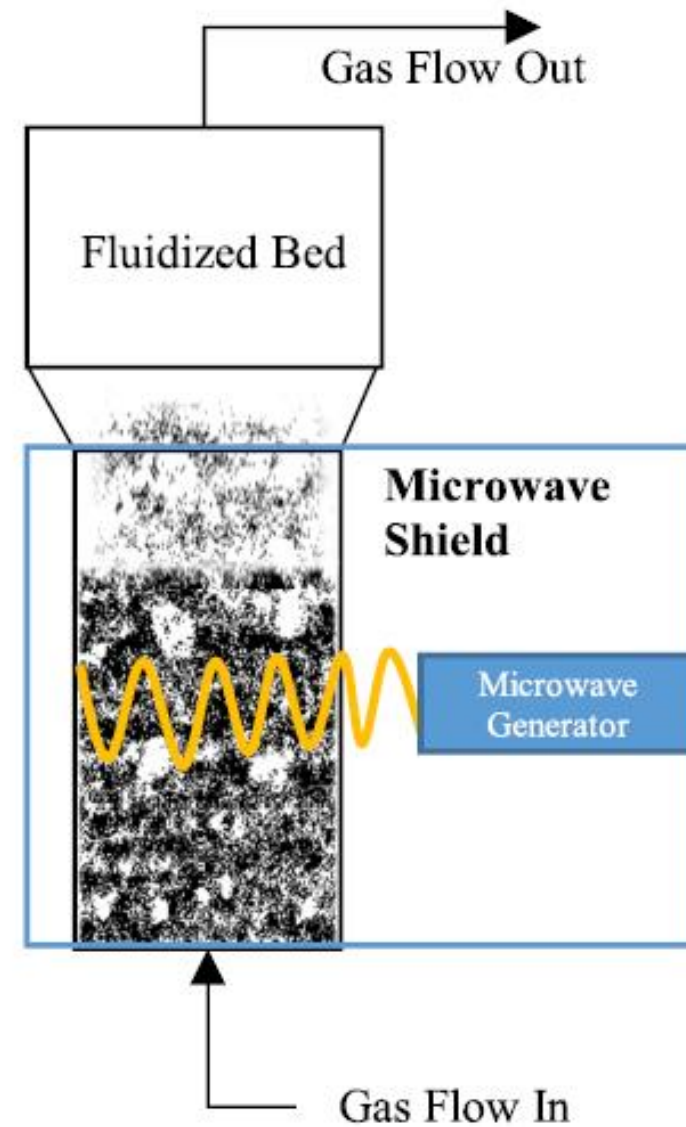
Wismann, et al. Ind. Eng. Chem. Res. 58 (2019) 23380

electrical heating

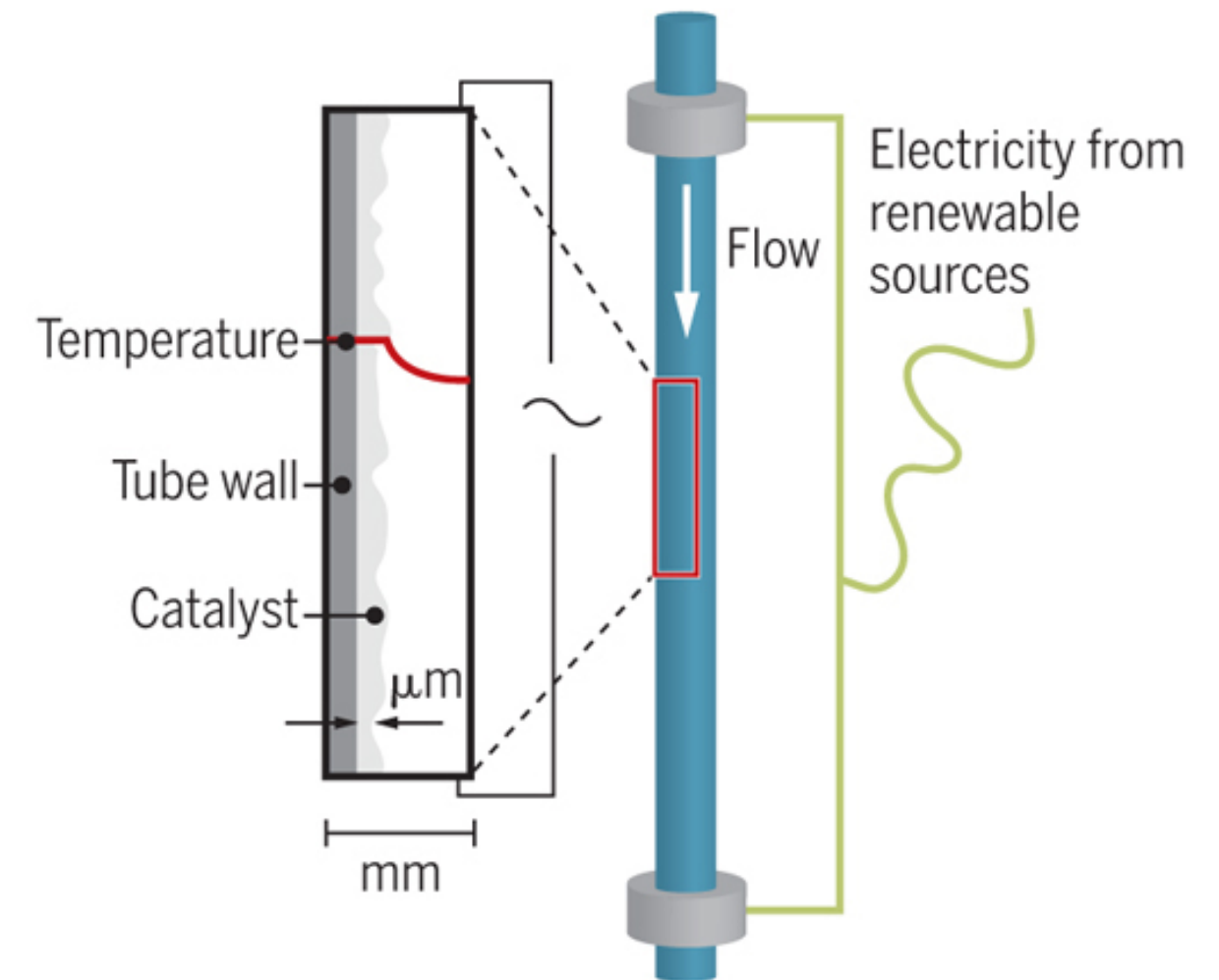
induction



microwave



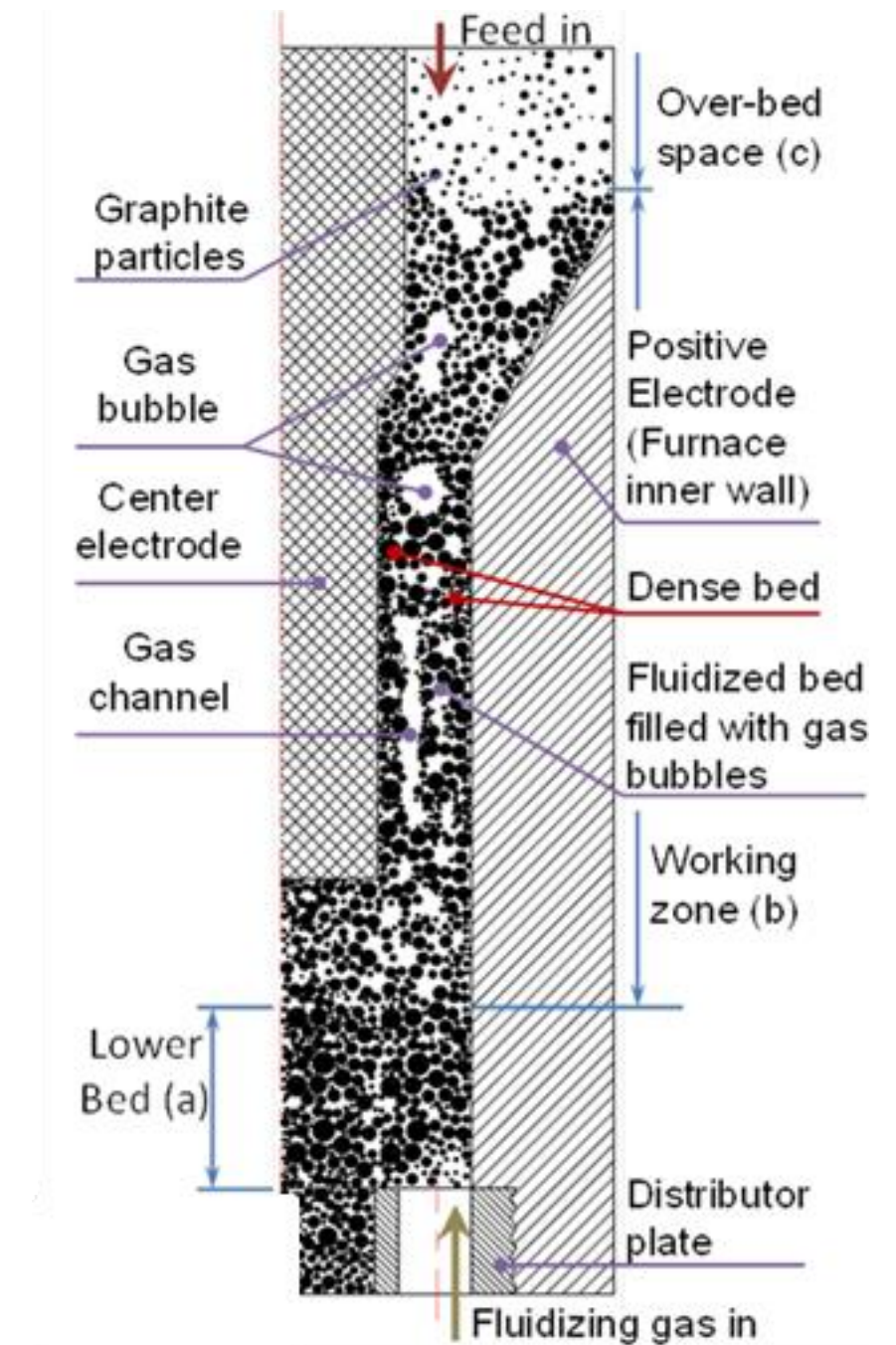
Joule



sonication plasma

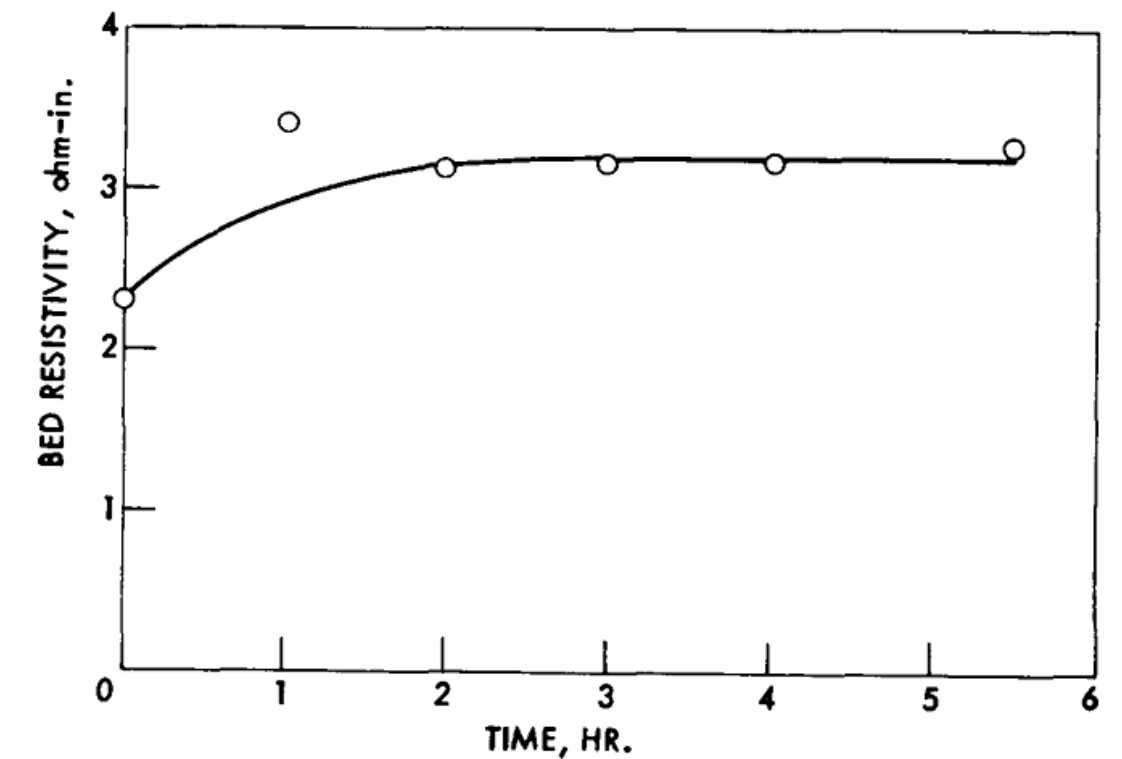
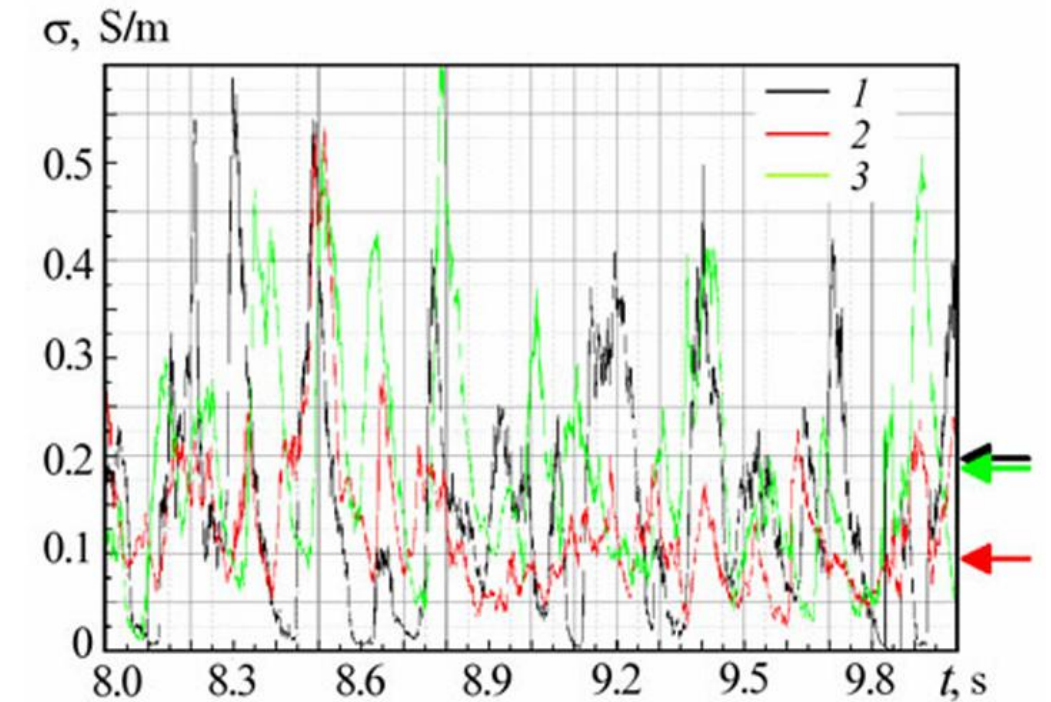
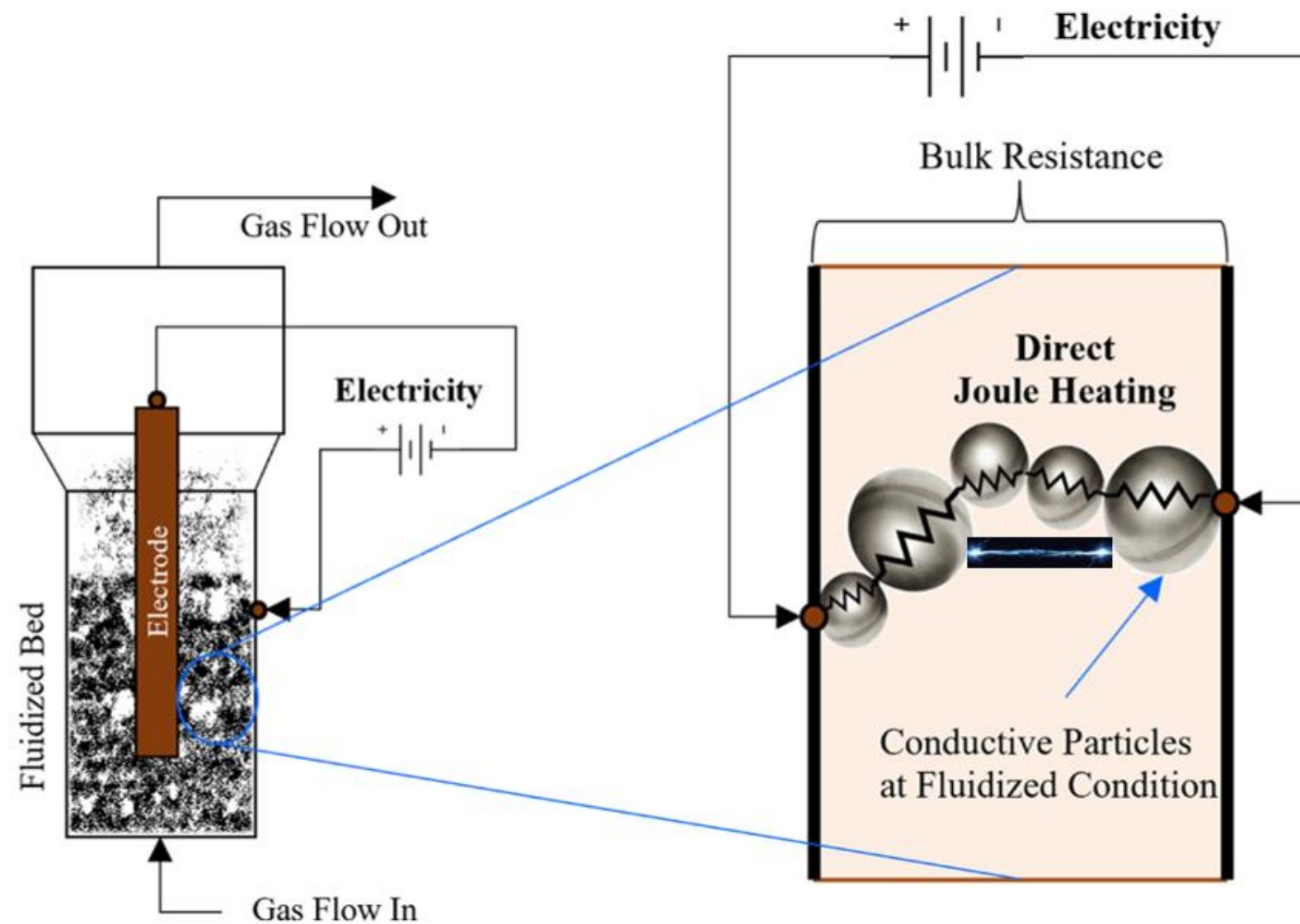
ElectroThermal Fluidized Bed reactor (ETFB)

- combination:
 - fluidization
 - Joule heating
- compared to conventional fluidized beds
 - better control over bed temperature
 - highly energy efficient
 - rapid and uniform heating



Fedorov J. Fluids Eng. 138 (2016) 044502

Joule heating in a fluidized bed



ETFB reactor mass balance

assumptions

- bubbling fluidization regime
- low- and high-density phases are at the same temperature
- no radial profiles
- constant effective conductivity at average temperature and composition
- adiabatic operation
- steady state operation

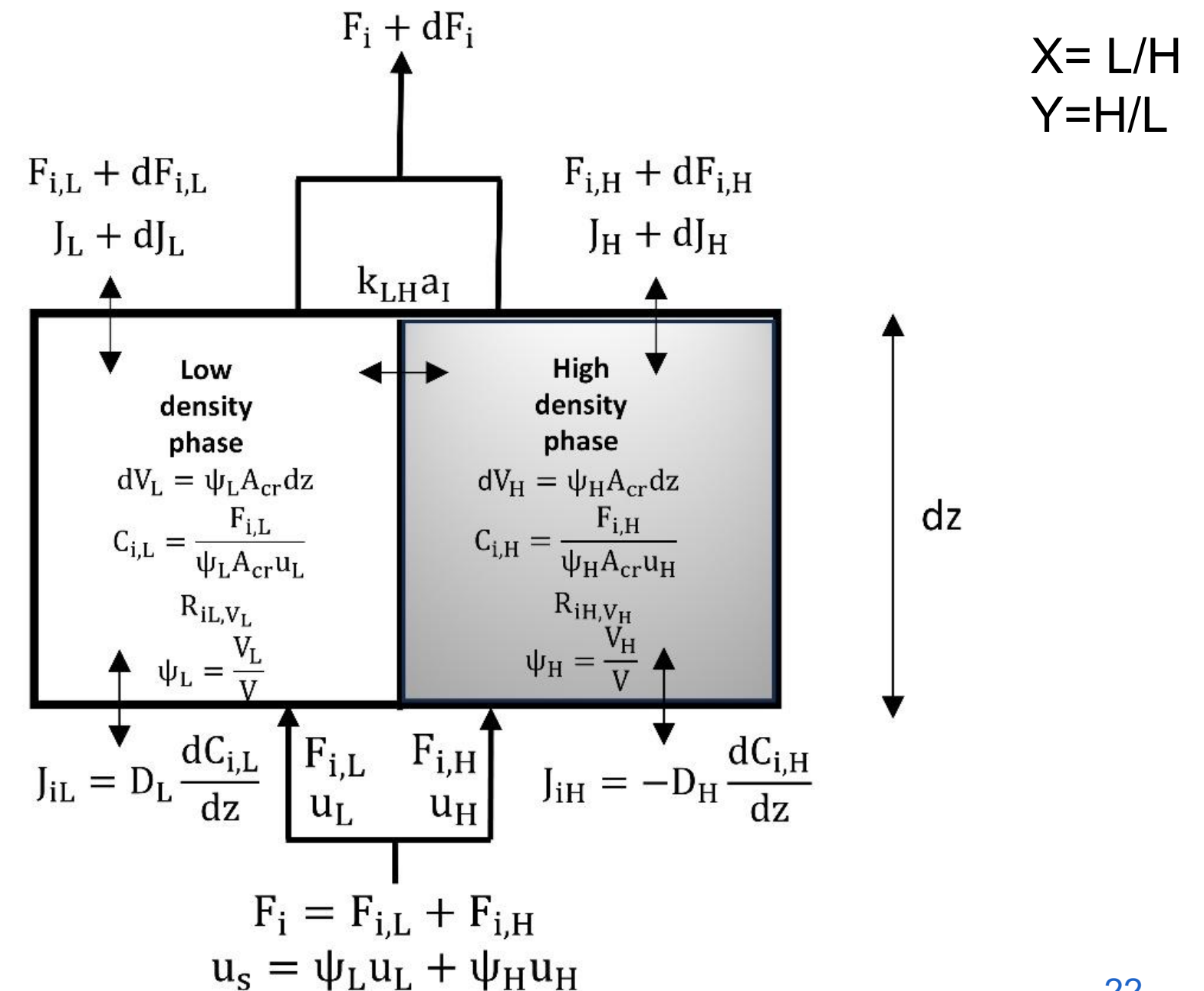
$$\frac{dF_{iX}}{dz} - \varepsilon_X R_{iX,V_X} \psi_X A_{cr} - \frac{D_X}{u_X} \frac{d^2 F_{i,X}}{dz^2} + k_{LH} a_I \psi_L \left(\frac{F_{iX}}{\psi_X u_X} - \frac{F_{iY}}{\psi_Y u_Y} \right) = 0$$

convection

reaction

diffusion

phase transfer



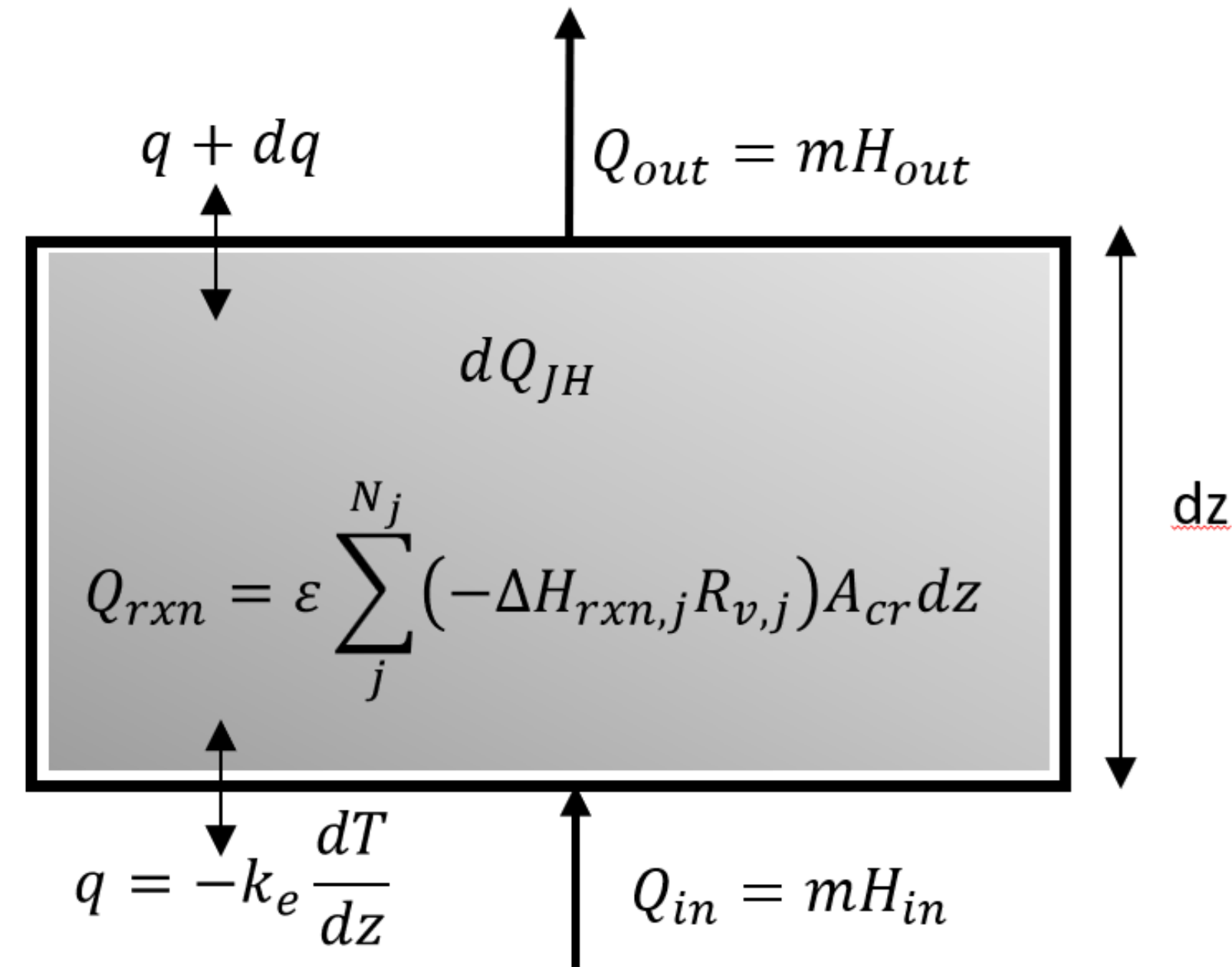
Jacobs et al. Chem. Eng. Sci. 2026 327 123647

ETFB reactor heat balance

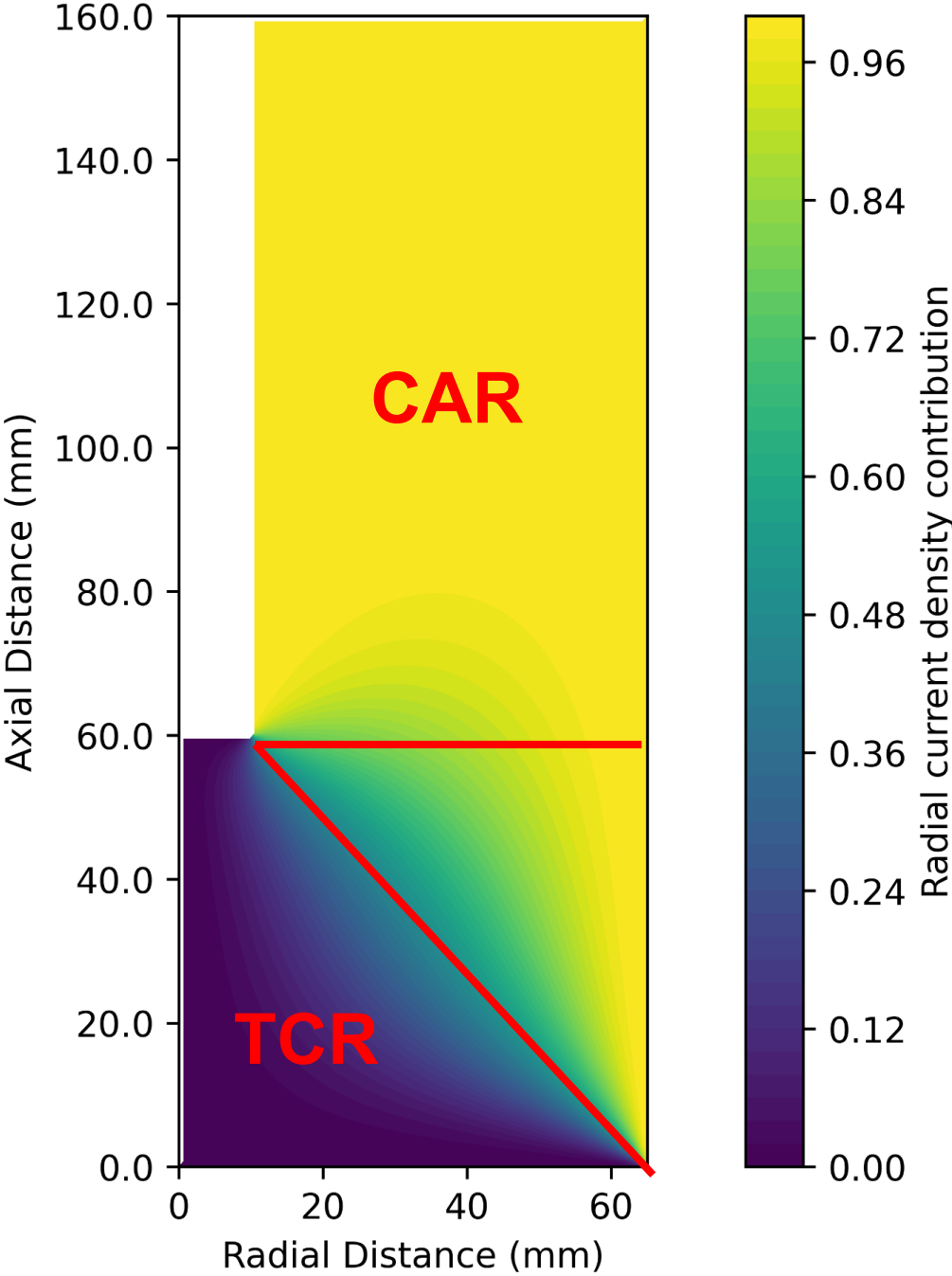
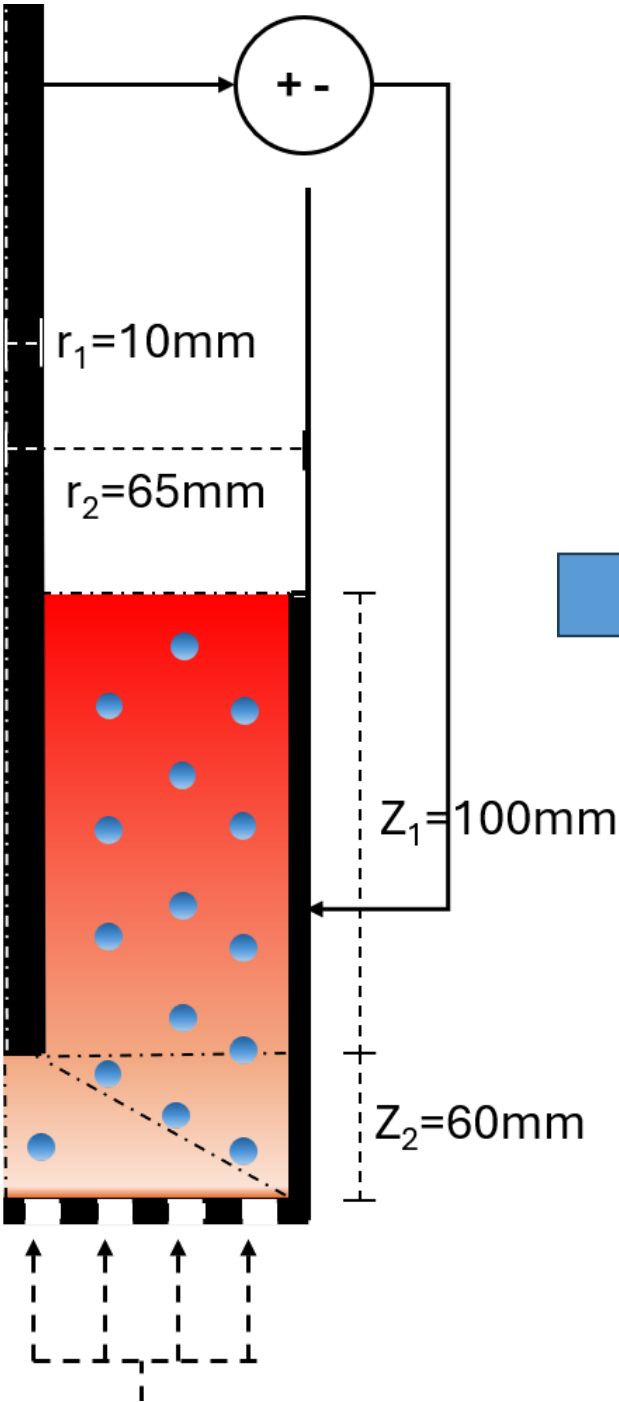
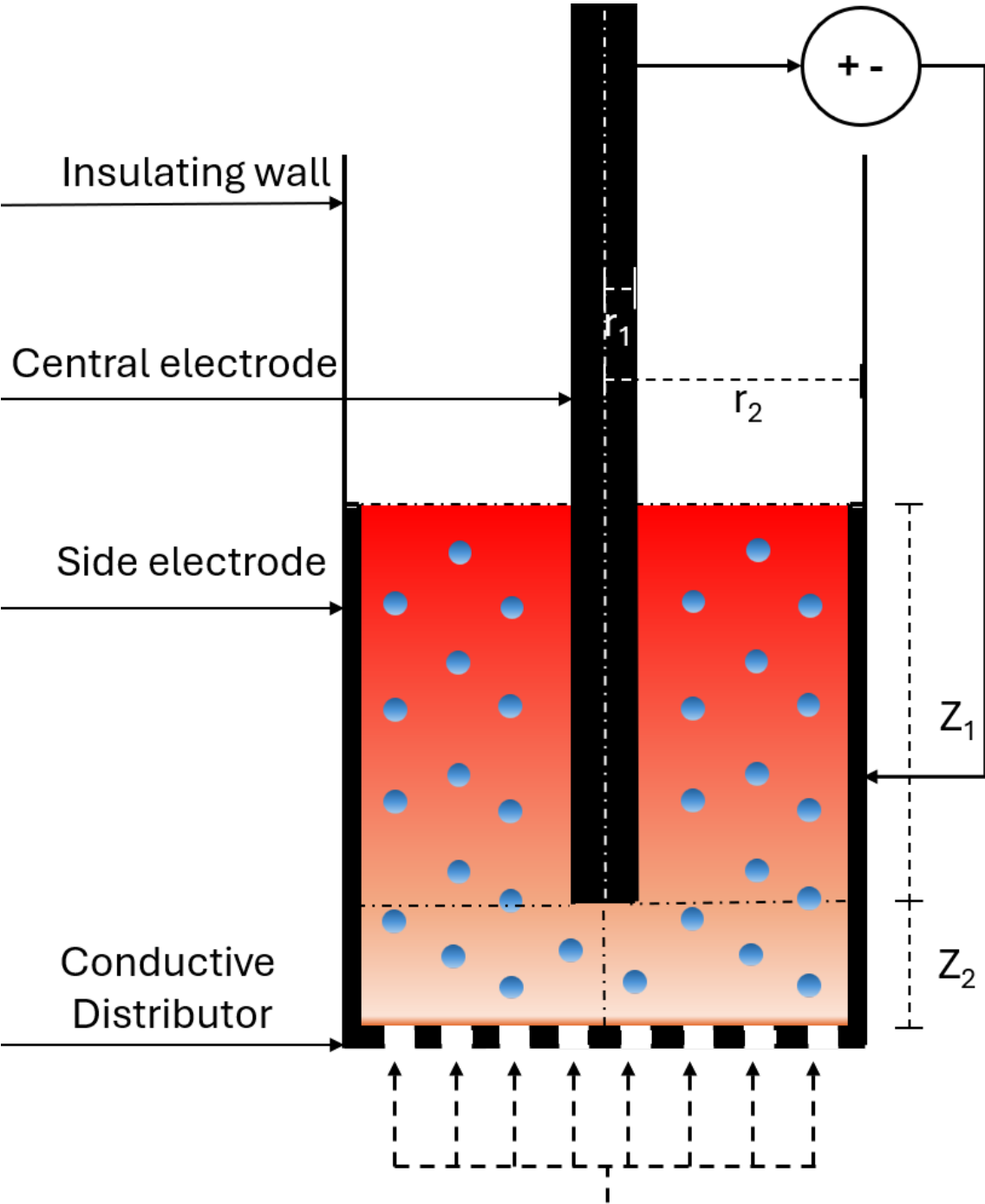
$$u\rho_g C p_g \frac{dT}{dz} - k_e \frac{d^2T}{dz^2} - \varepsilon \sum_j^{N_j} (-\Delta H_{rxn} R_{v,j}) - \frac{dQ_{JH}}{dz A c_{reactor}} = 0$$

convection conduction heat of reaction heat generation
 → Joule heating term

electrical field calculation



ETFB electrical field



truncated cone resistor

ETFB resistance

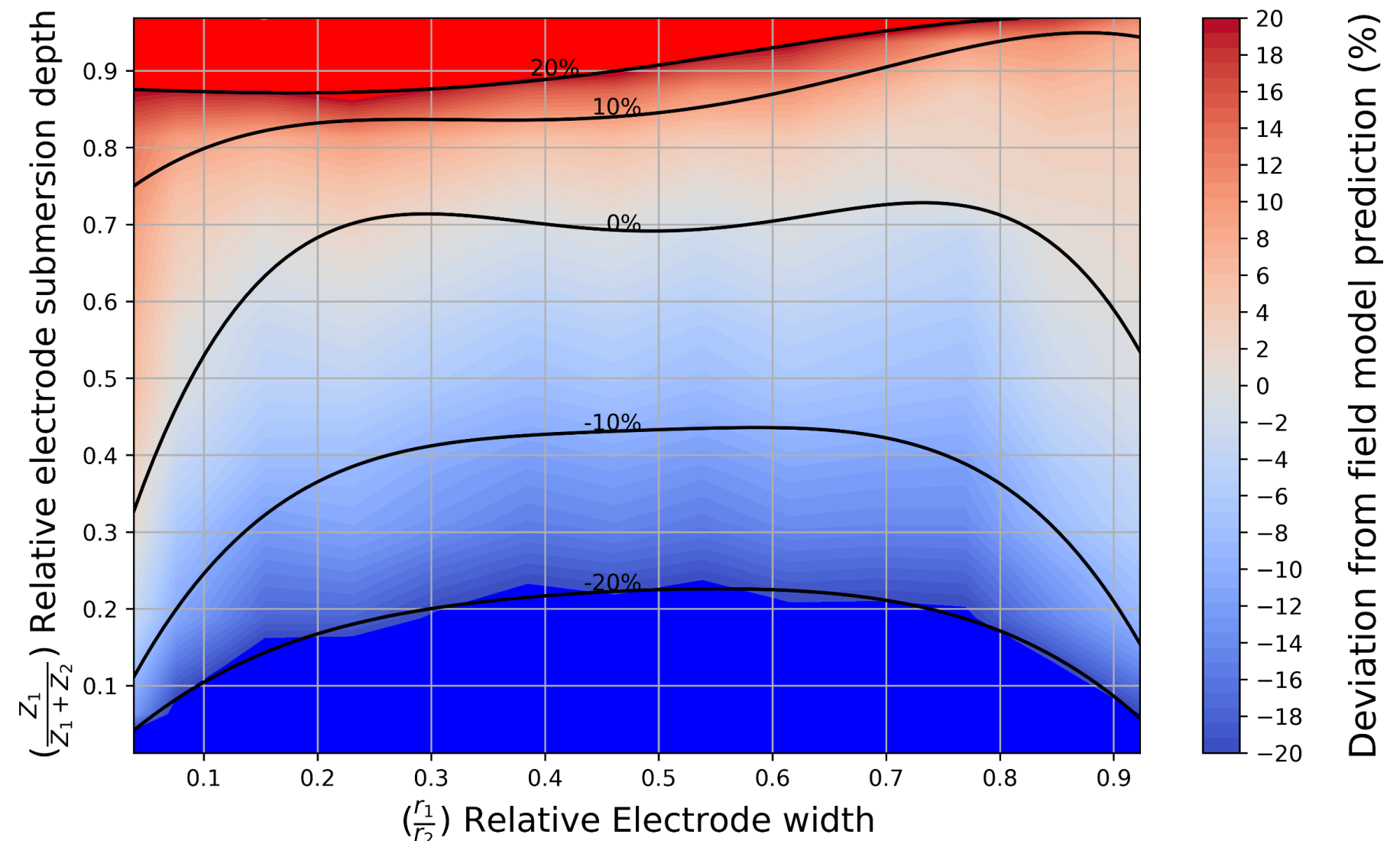
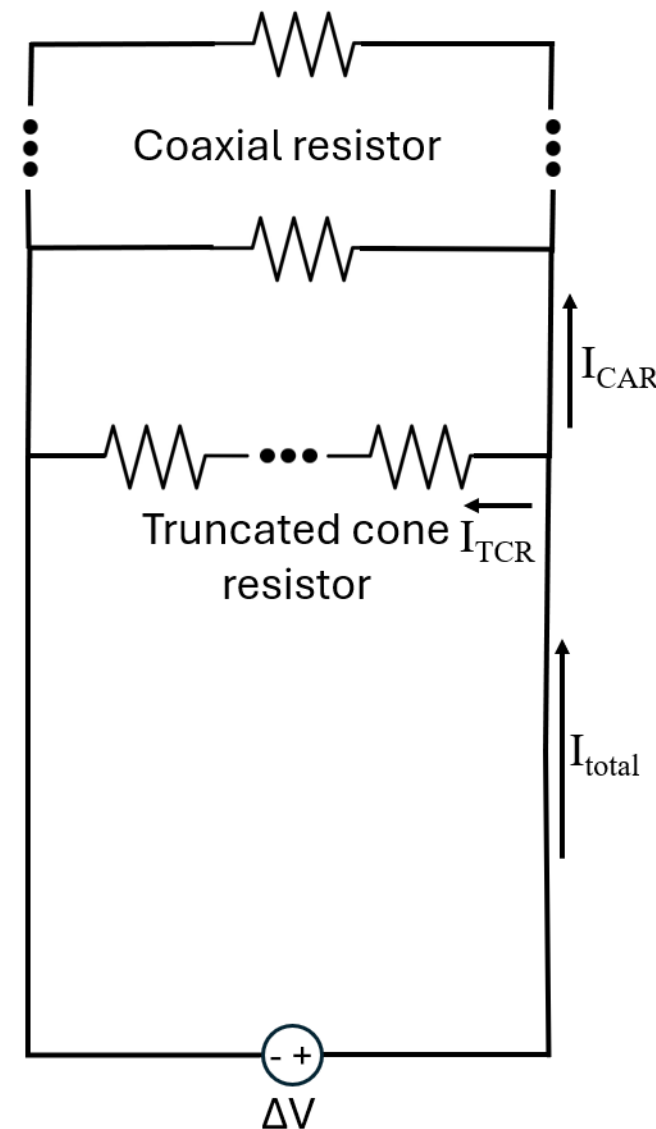
assuming contact resistances with the electrodes are negligible



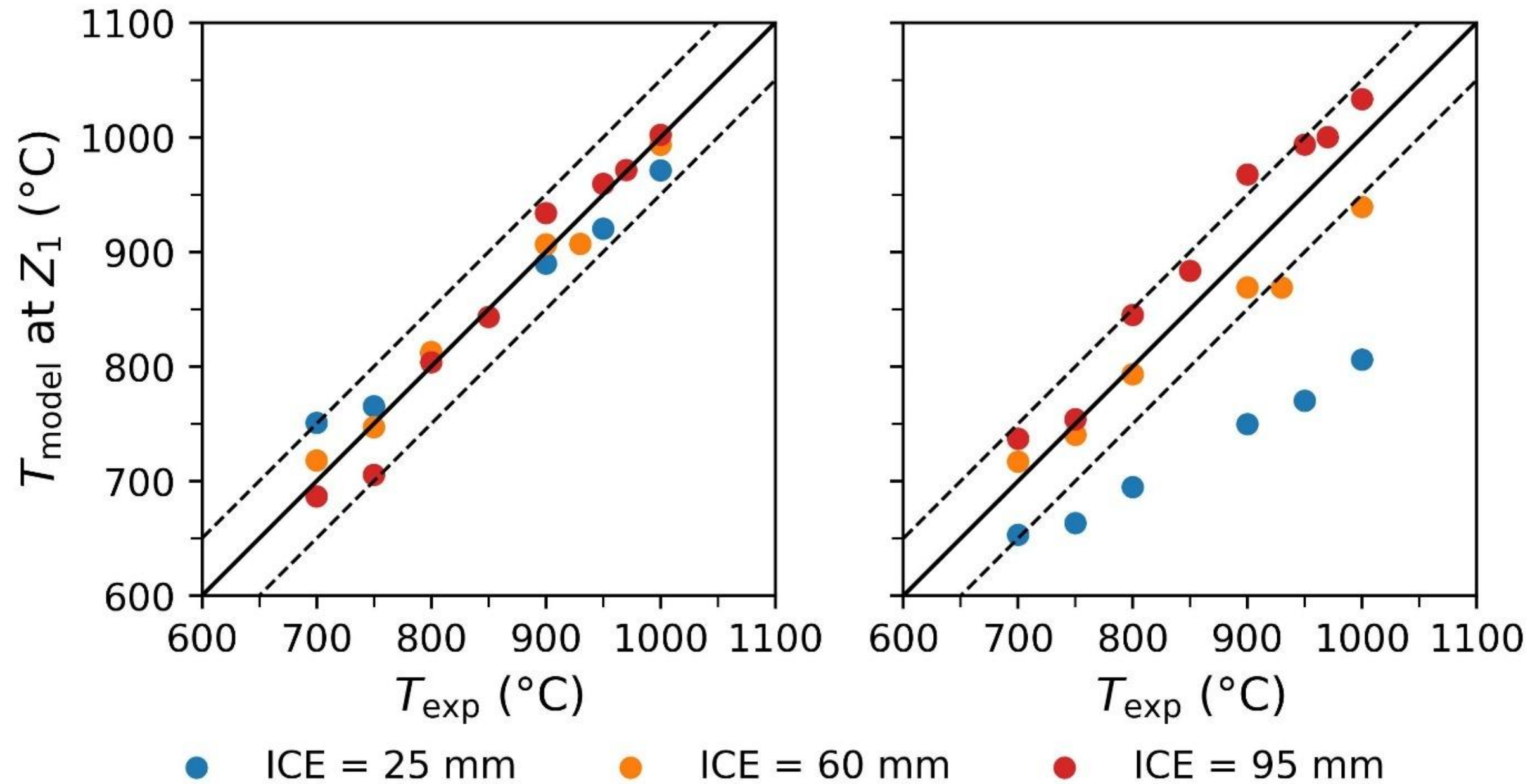
CARs and TCRs are represented as two resistors in parallel

$$R_{total} = \left(\frac{1}{R_{CAR}} + \frac{1}{R_{TCR}} \right)^{-1}$$

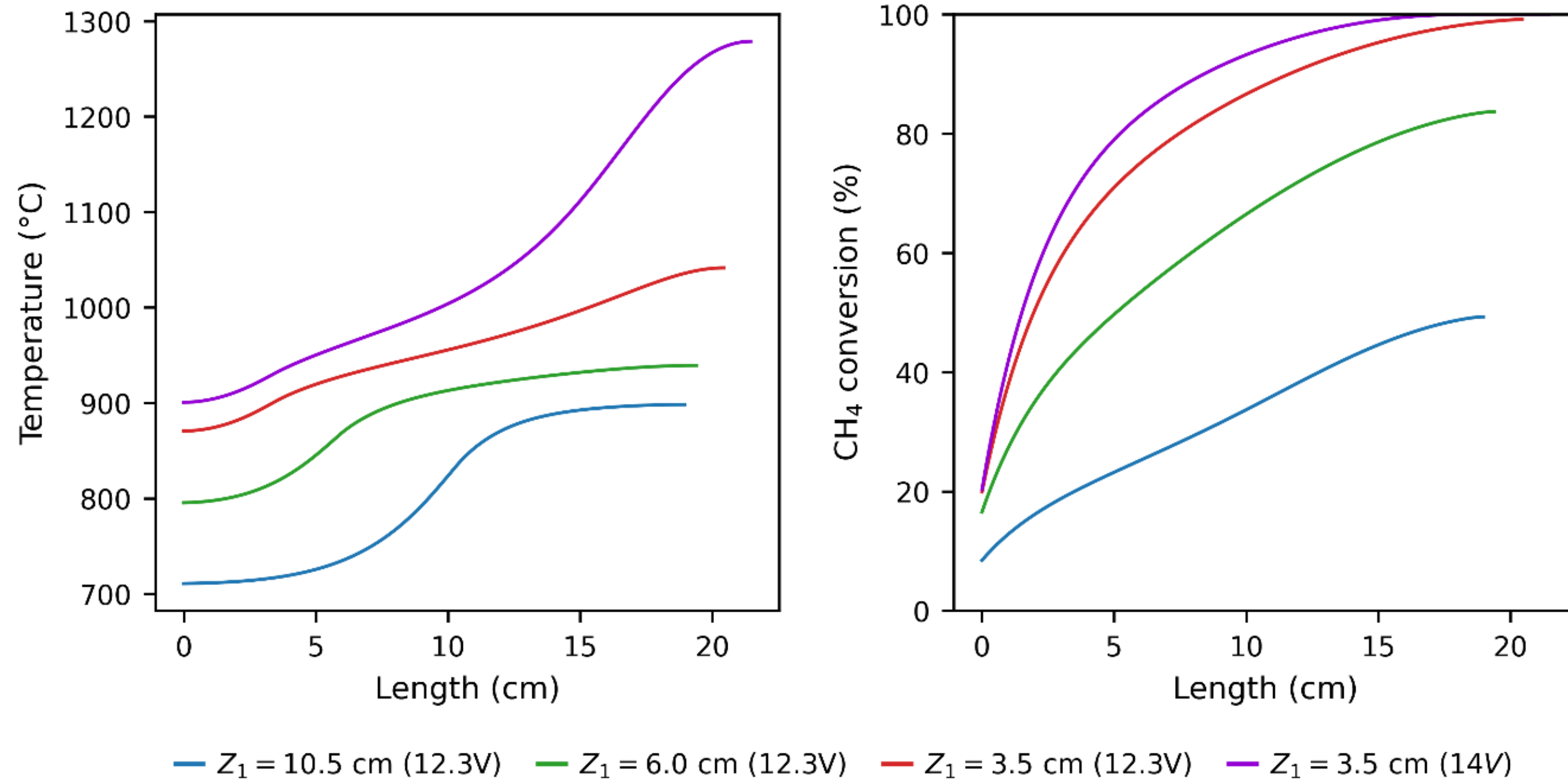
$$Q_{JH,total} = \frac{V^2}{R_{total}} = I_{total}^2 R_{total} = V I_{total}$$



thermal model validation



methane pyrolysis performance simulation



ETFB reactor set-up



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conclusions and perspectives

- “electricity is in the catalyst”
 - reactor electrification not just connecting electric heater to the grid
 - reasoning from the inside: ElectroThermal Fluidized Bed (ETFB) reactor
 - opportunities for endothermic reactions
- methane pyrolysis
 - crucial role of surface area: it increases H radical formation (and methyl radical formation in the gas phase)
 - higher hydrogen purity already at lower temperatures
 - higher temperature/higher space time required to compensate for deactivation

conclusions and perspectives

- ETFB reactor
 - electrode submersion enhances heat generation
 - temperature excursions in case of full conversion

acknowledgments

Interreg



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OBIWAN

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Marie-Elisabeth Lissens

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LABORATORY FOR CHEMICAL TECHNOLOGY

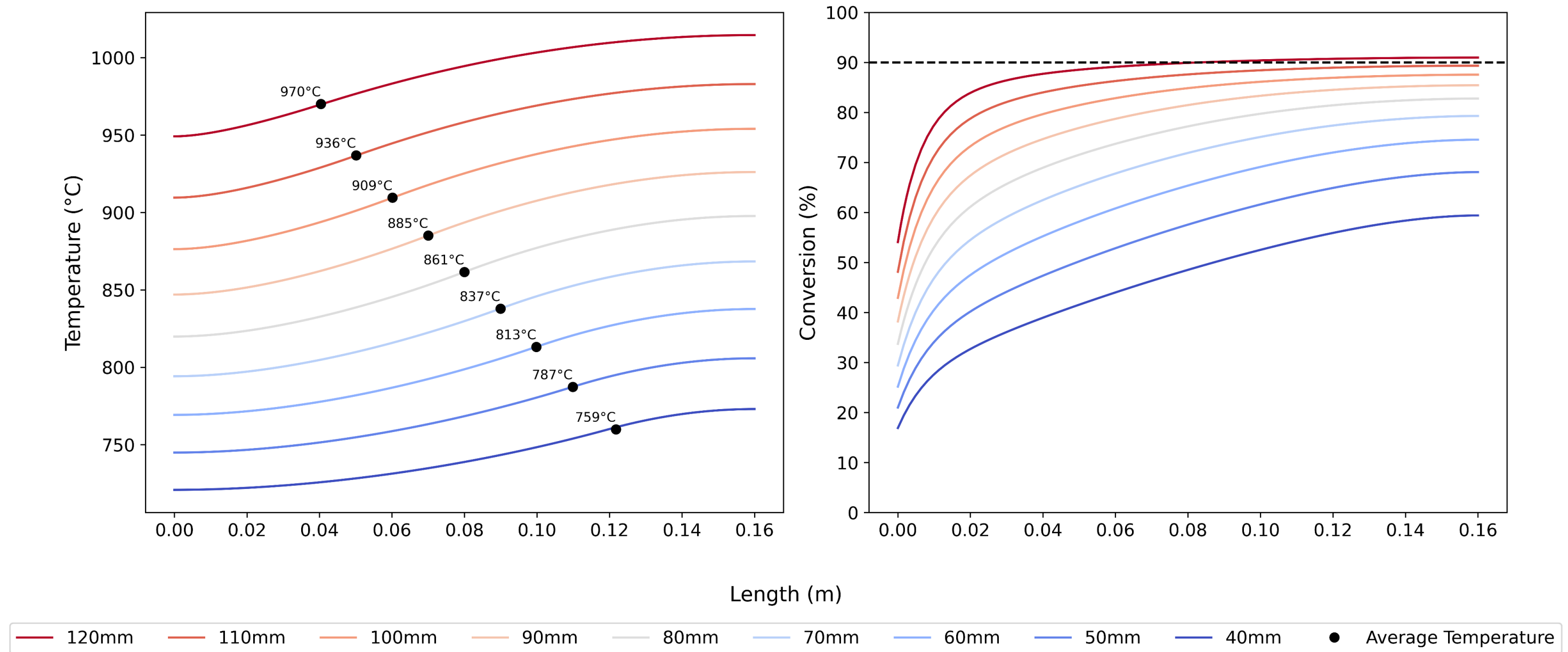
Technologiepark 125, 9052 Ghent, Belgium

E info.lct@ugent.be

T 003293311757

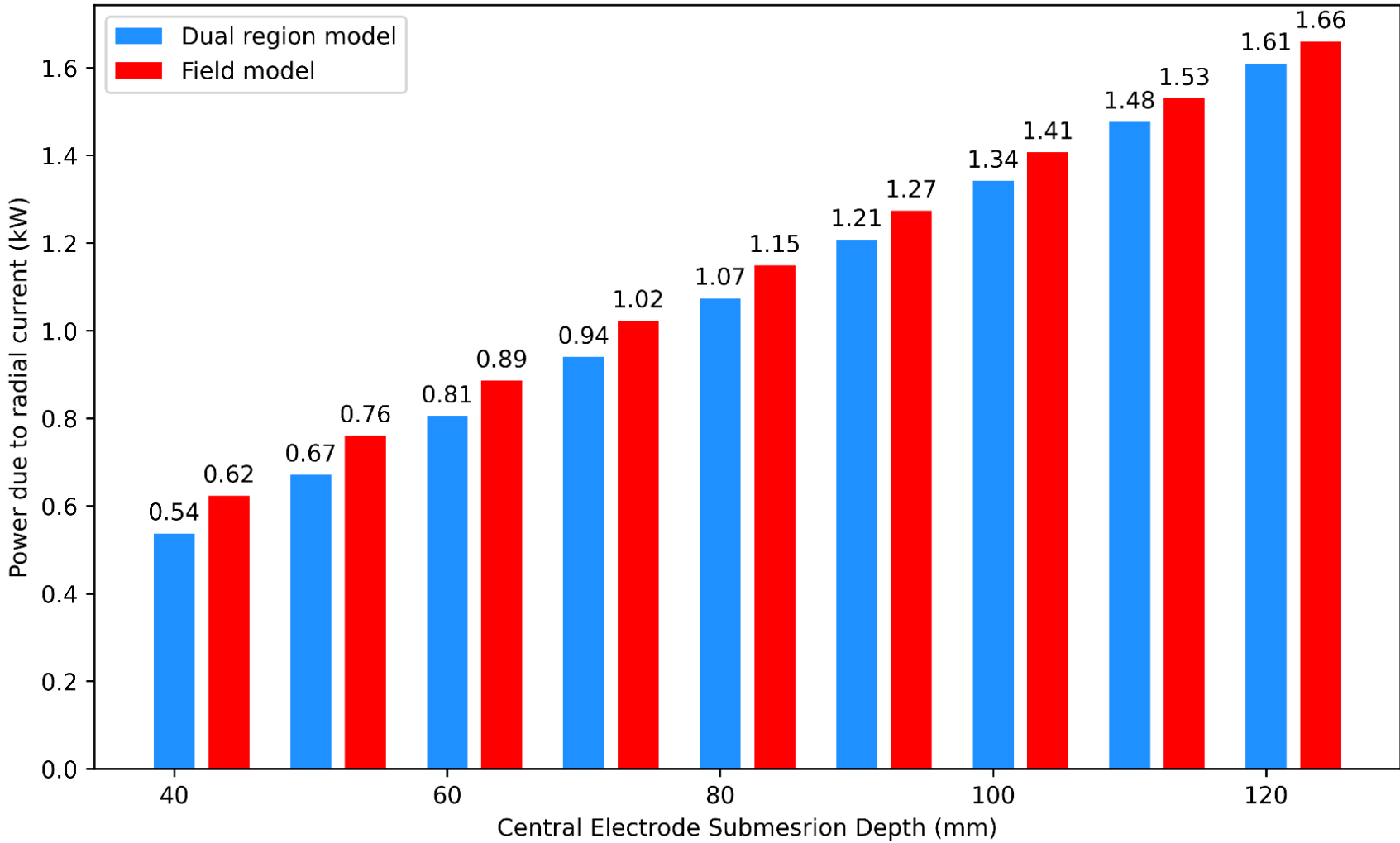
<https://www.lct.ugent.be>

e-CODUCT – ETFB simulation

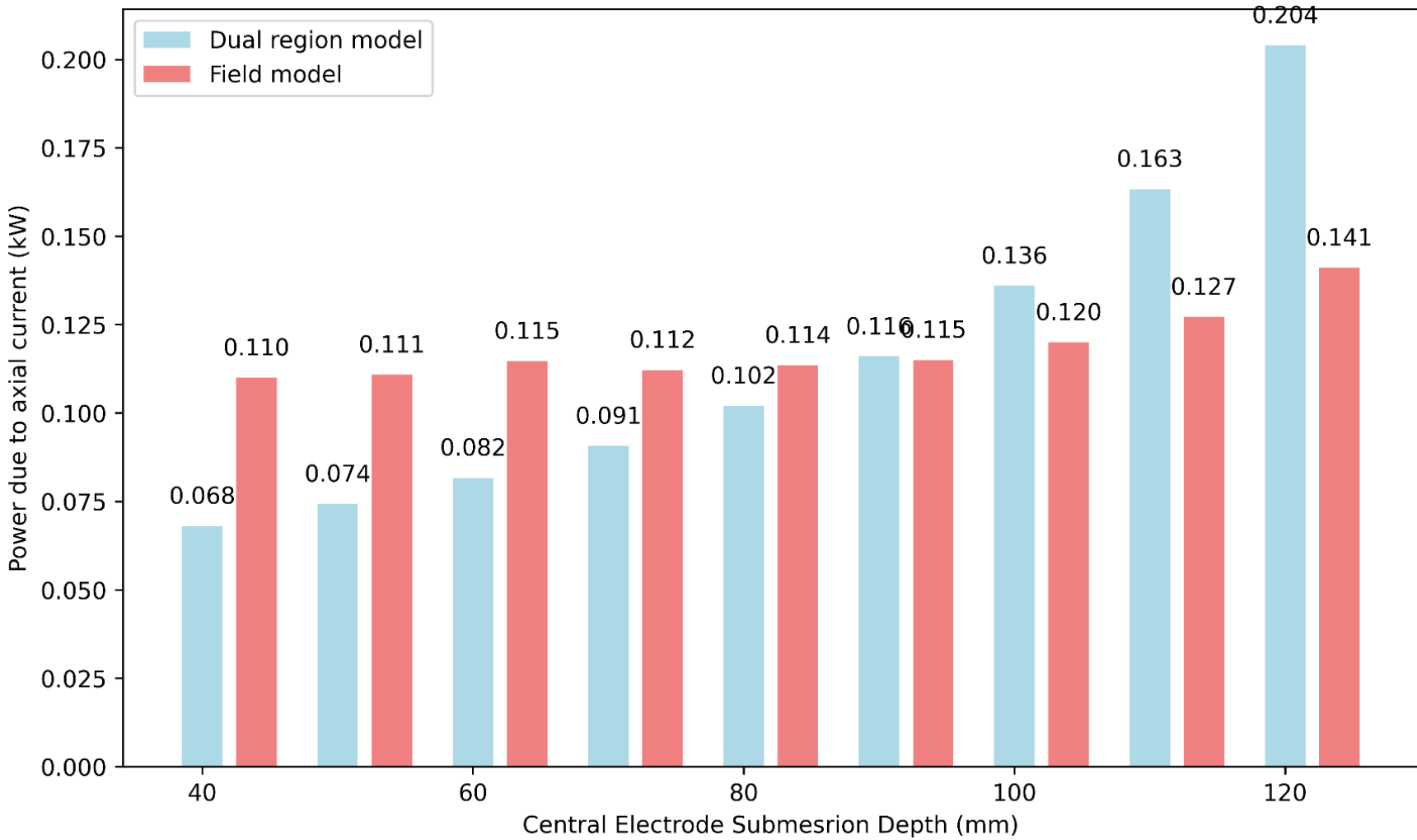


axial temperature (left) and COS conversion (right) profile as function of length for different electrode submersion depth.

2 zone vs field model simulations



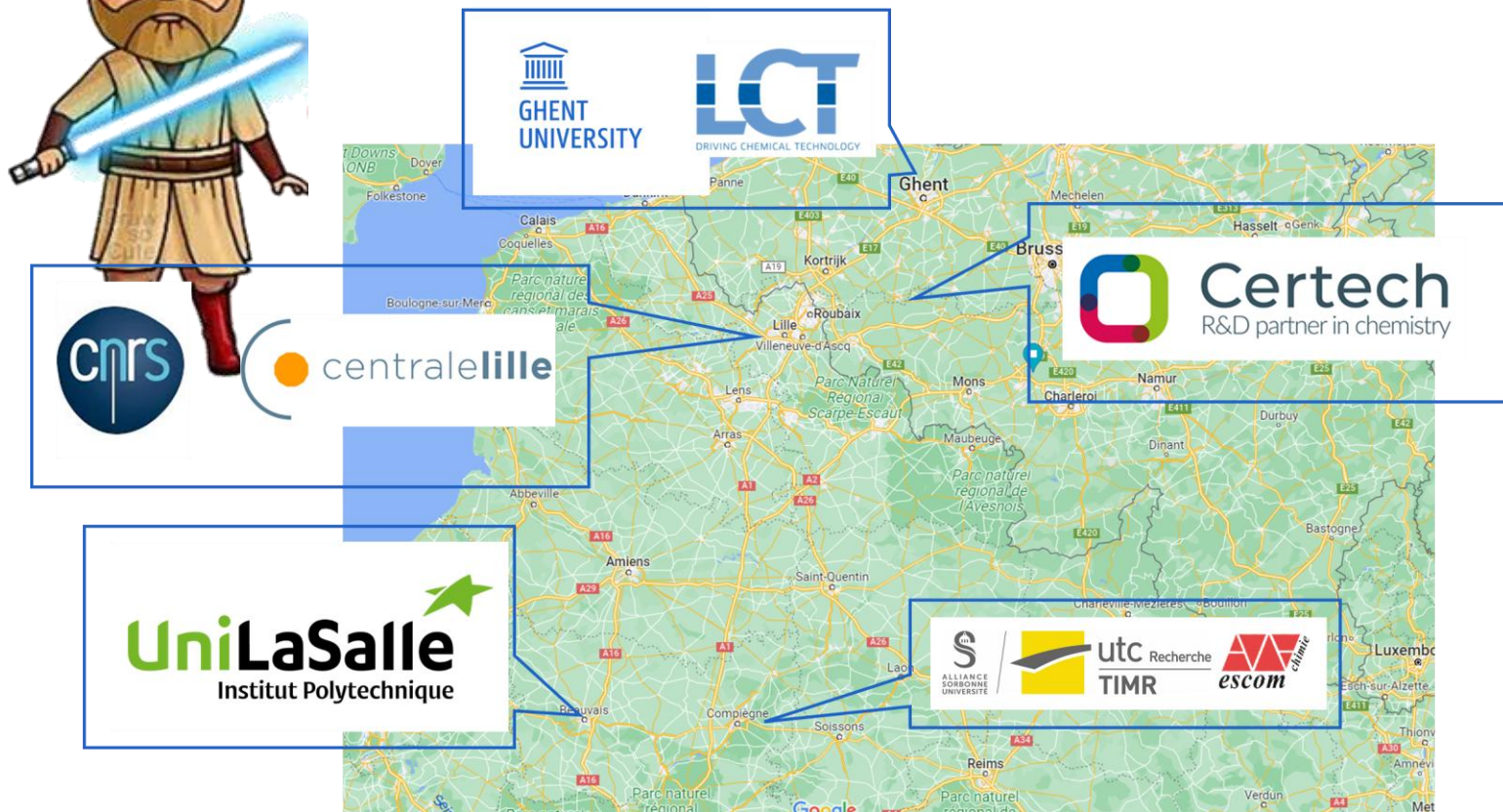
coaxial resistor (CAR)



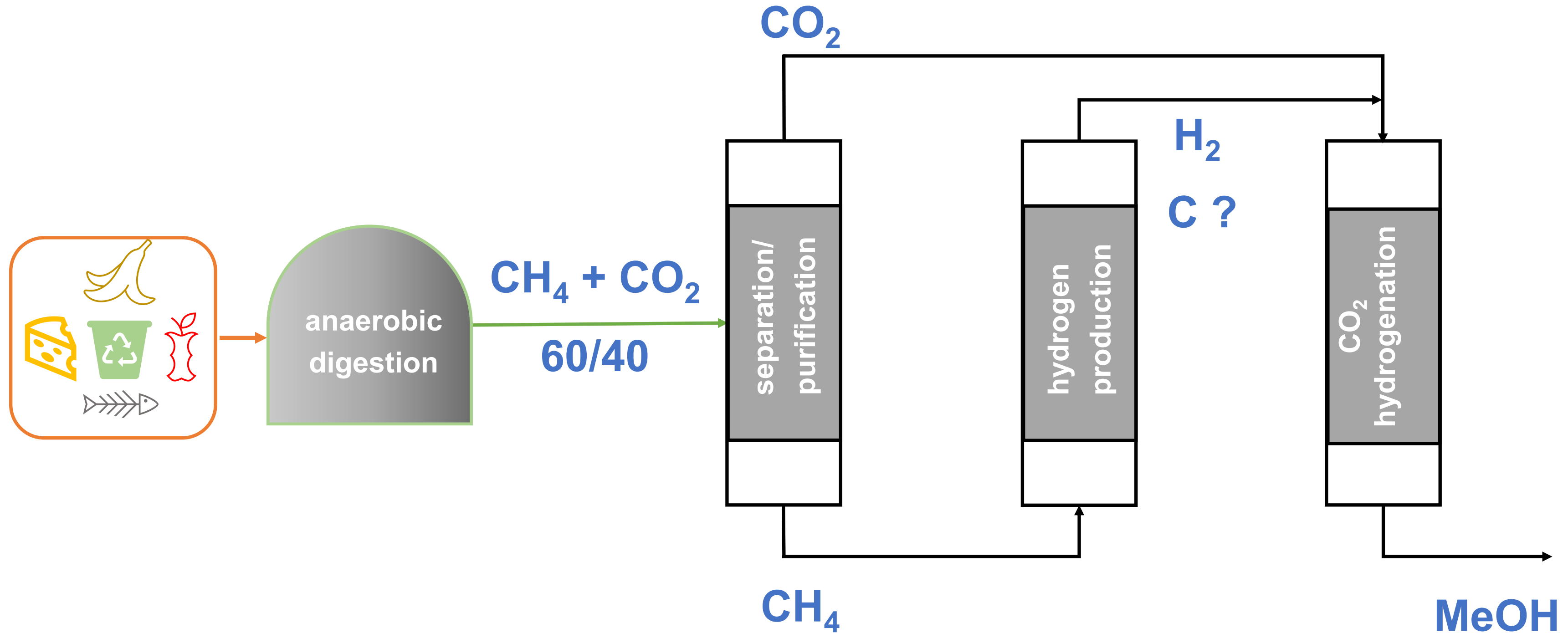
truncated cone resistor (TCR)

OBIWAN: context

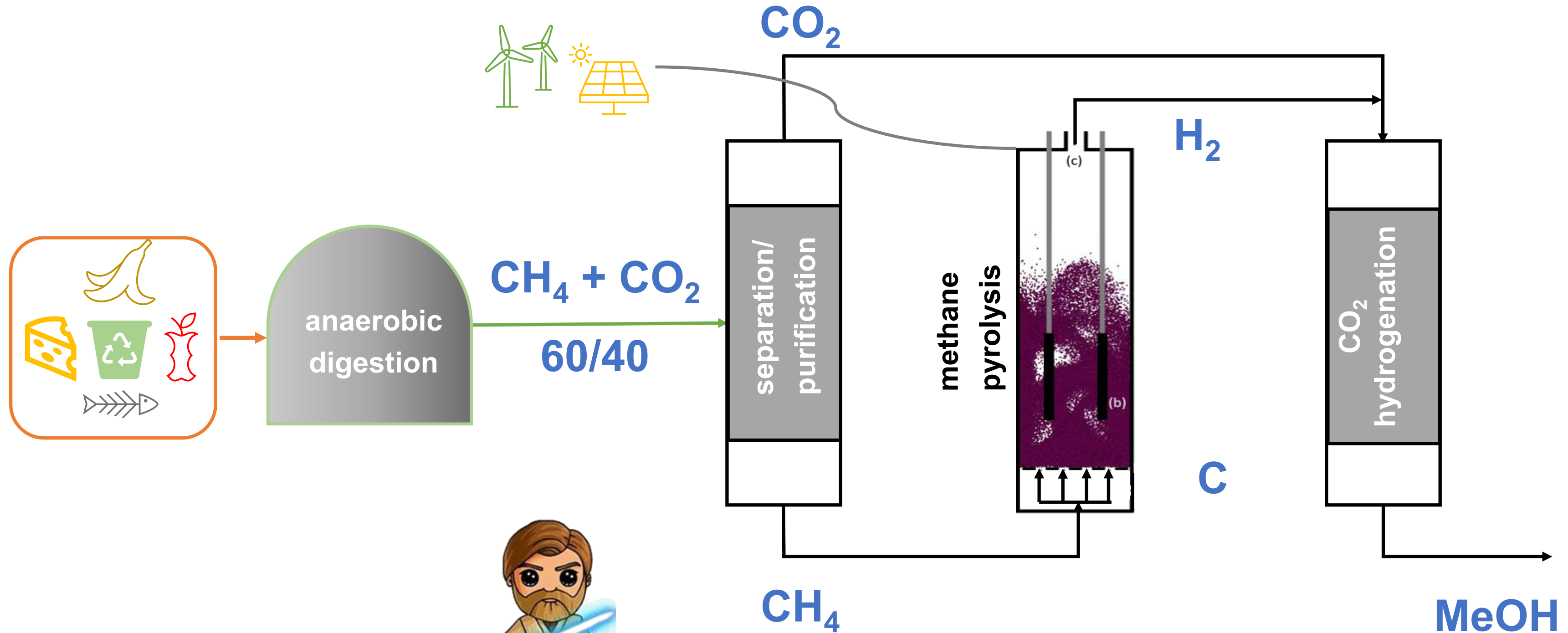
- biogas ($\text{CH}_4 + \text{CO}_2$) valorization
 - calorific
 - to chemicals/(sustainable aviation fuels)



OBIWAN: process lay-out



OBIWAN: process lay-out



OBIWAN start: October 2024